

# Summary of Rectangular Supercritical Wing (RSW) Analyses

David M. Schuster  
NASA Langley Research Center

Aeroelastic Prediction Workshop

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Honolulu, Hawaii

Notes: These comparisons are utilizing the preliminary data, as submitted prior to the AePW. These are workshop results, not publication results. There are significant differences in the geometry used, as well as normalization constants, definitions of FRF and sign conventions. These issues are being sorted out post-workshop. None of the results included should be interpreted without proper consideration of these issues. Corrections and rescalings etc will be performed prior to publication.

# RSW Data Submissions

Analyst	Organization
Pawel Chwalowski	NASA
Thorsten Hansen	ANSYS Germany GMBH
Dimitri Mavriplis	University of Wyoming
David Schuster	NASA
Daniel Steiling	RUAG Schweiz AG
Sebastian Timme	University of Liverpool



# Rectangular Supercritical Wing (RSW)



**$M=0.825$ ,  $Re_c=4.0$  million, test medium: R-12**

**a) Steady Cases**

i.  $\alpha = 2^\circ$

ii.  $\alpha = 4^\circ$

**b) Dynamic Cases**

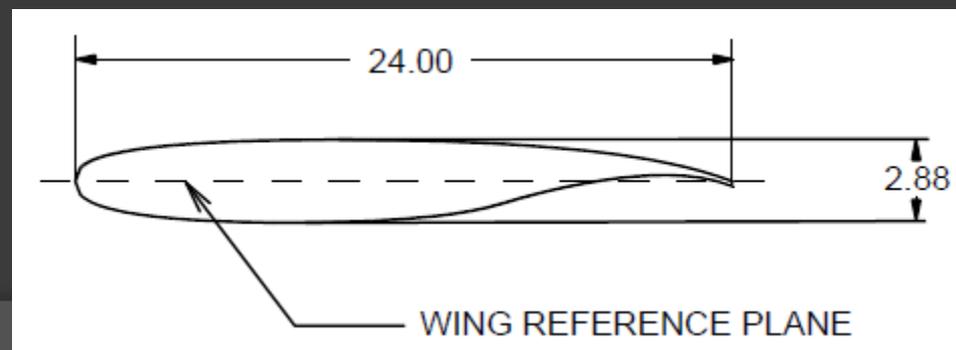
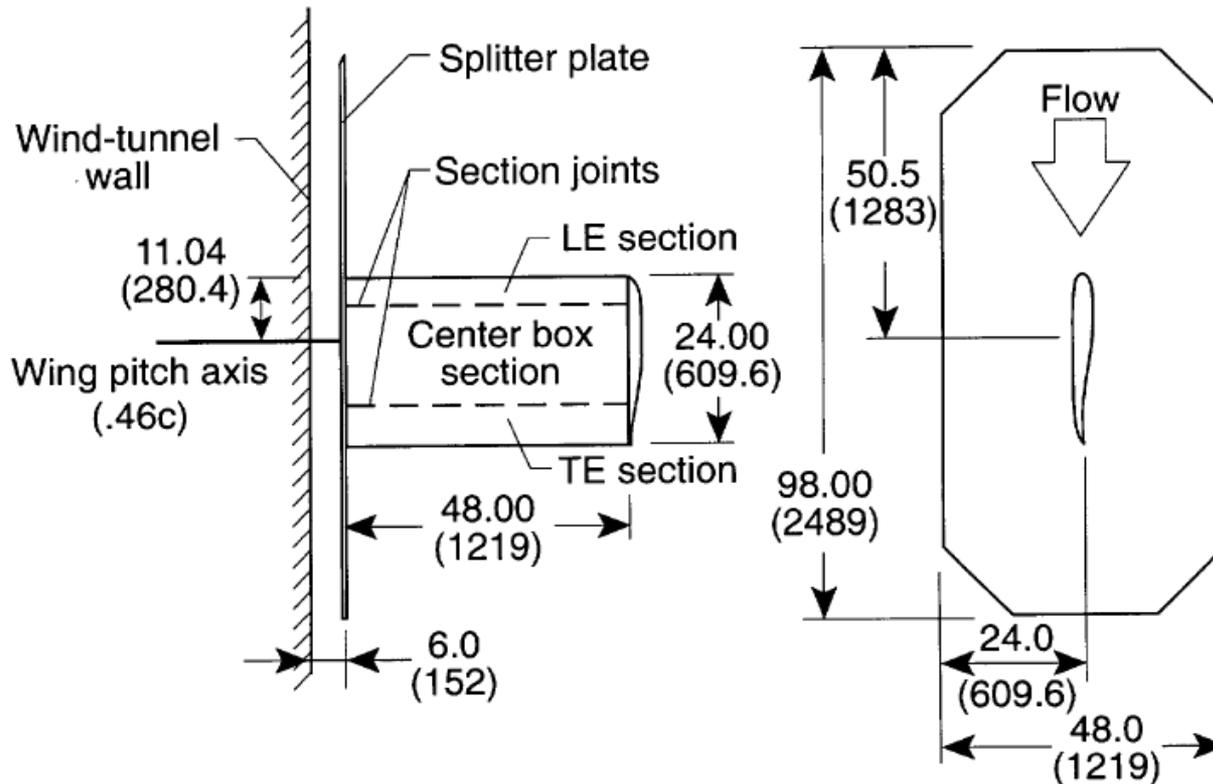
i.  $\alpha = 2^\circ$ ,  $\theta = 1.0^\circ$ ,  $f = 10$  Hz

ii.  $\alpha = 2^\circ$ ,  $\theta = 1.0^\circ$ ,  $f = 20$  Hz

# RSW Modeling Considerations

- ⦿ Close proximity of splitter plate to wind tunnel sidewall resulted in plate being immersed in tunnel wall boundary layer.
- ⦿ Study conducted to determine most expedient approach to solve this problem.

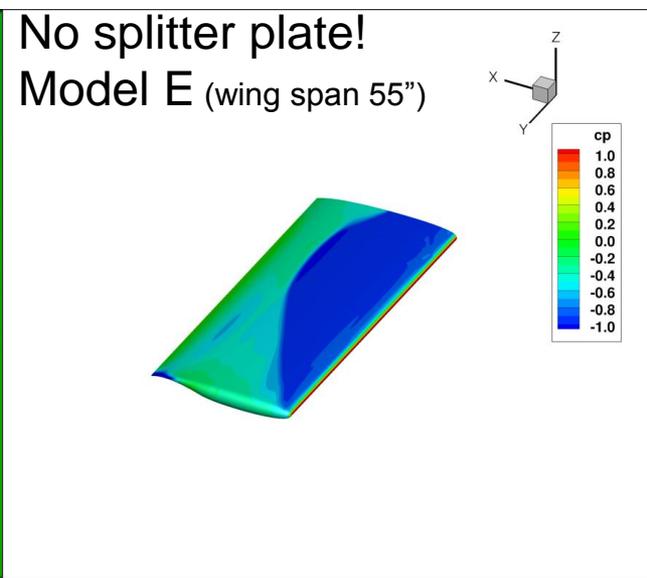
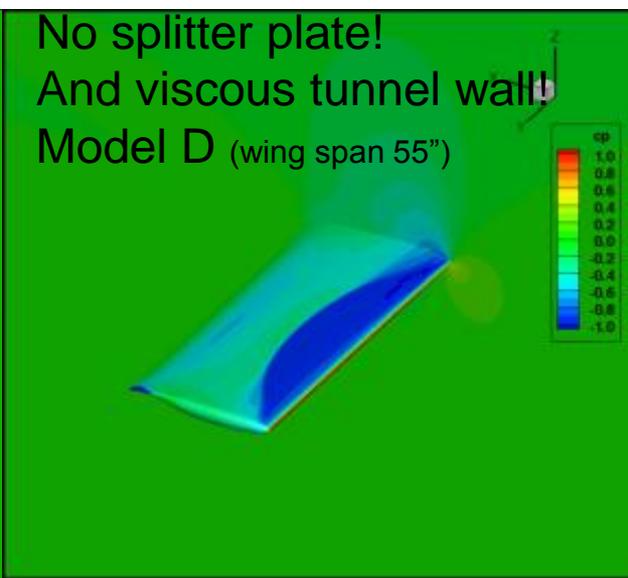
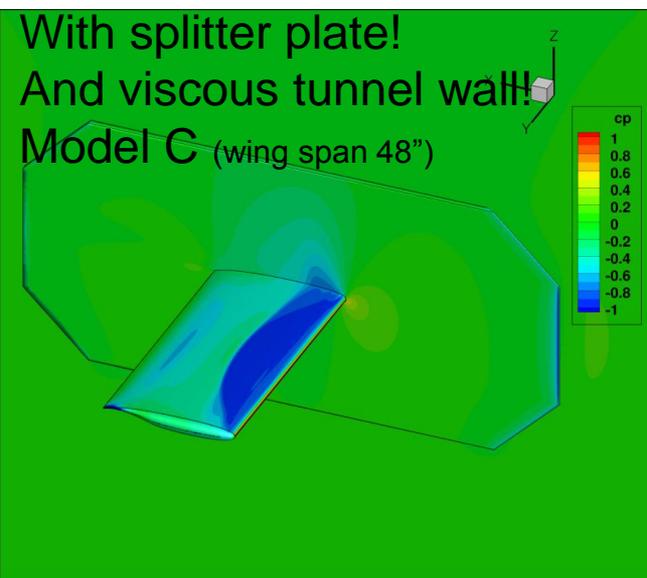
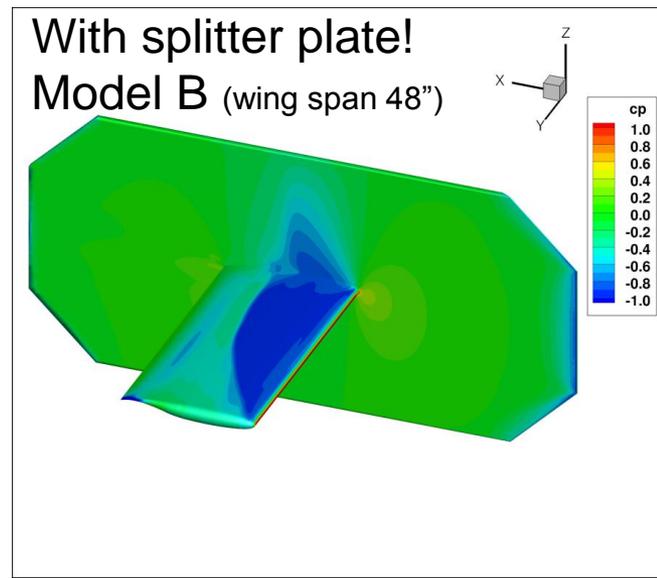
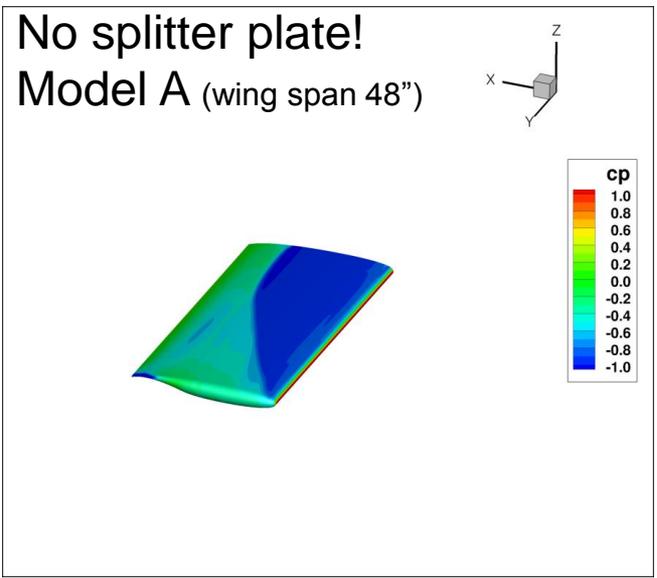
# RSW Model Layout and Airfoil





# Preliminary RSW Analysis Update

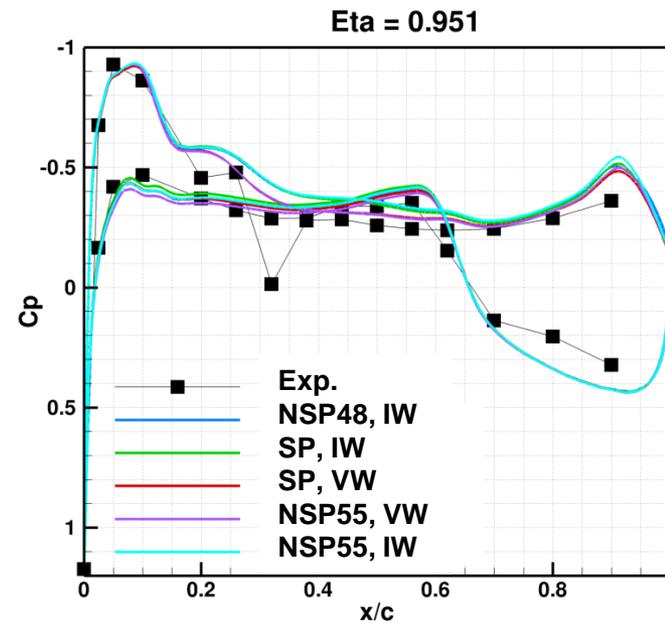
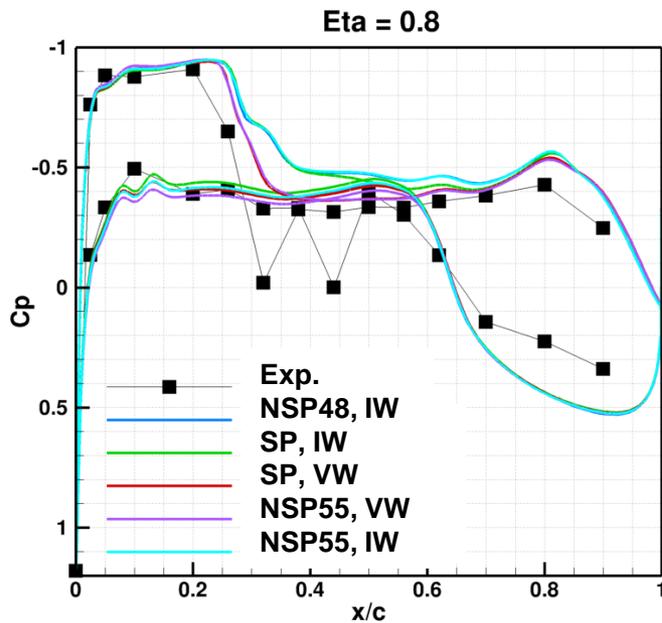
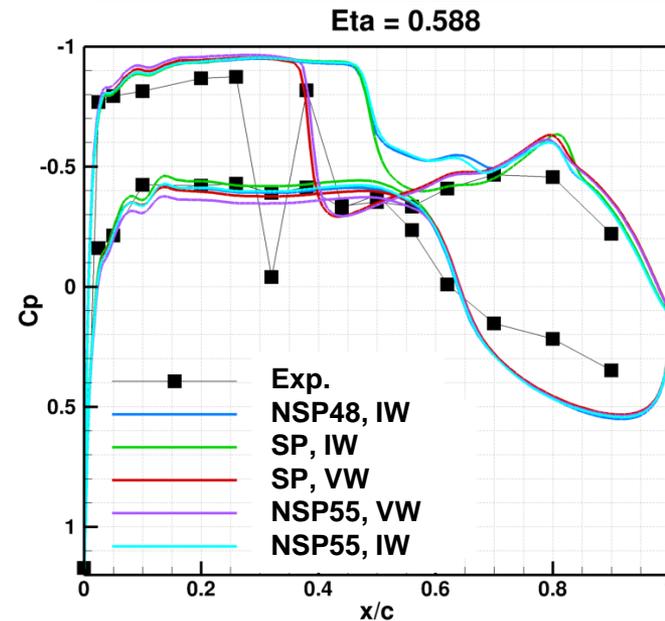
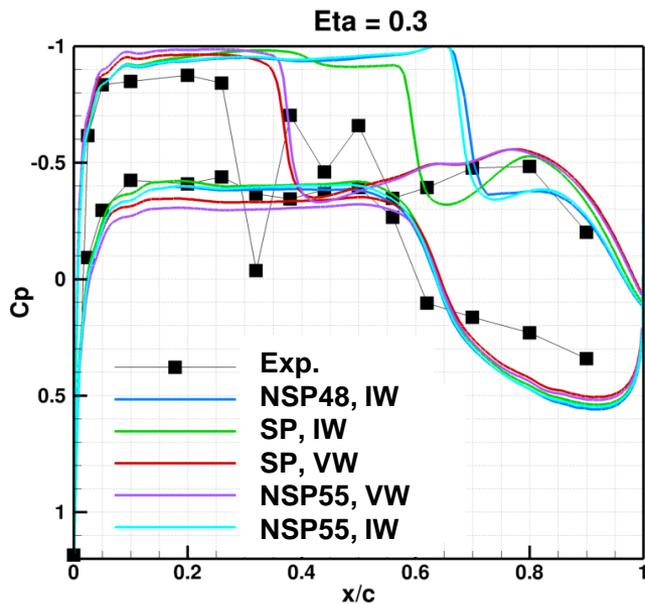
Mach = 0.825,  $\alpha = 2^\circ$ , Medium Grid Resolution





# Preliminary RSW Analysis Update

Mach = 0.825, AoA = 2deg, FUN3D vs. Steady Experimental Data



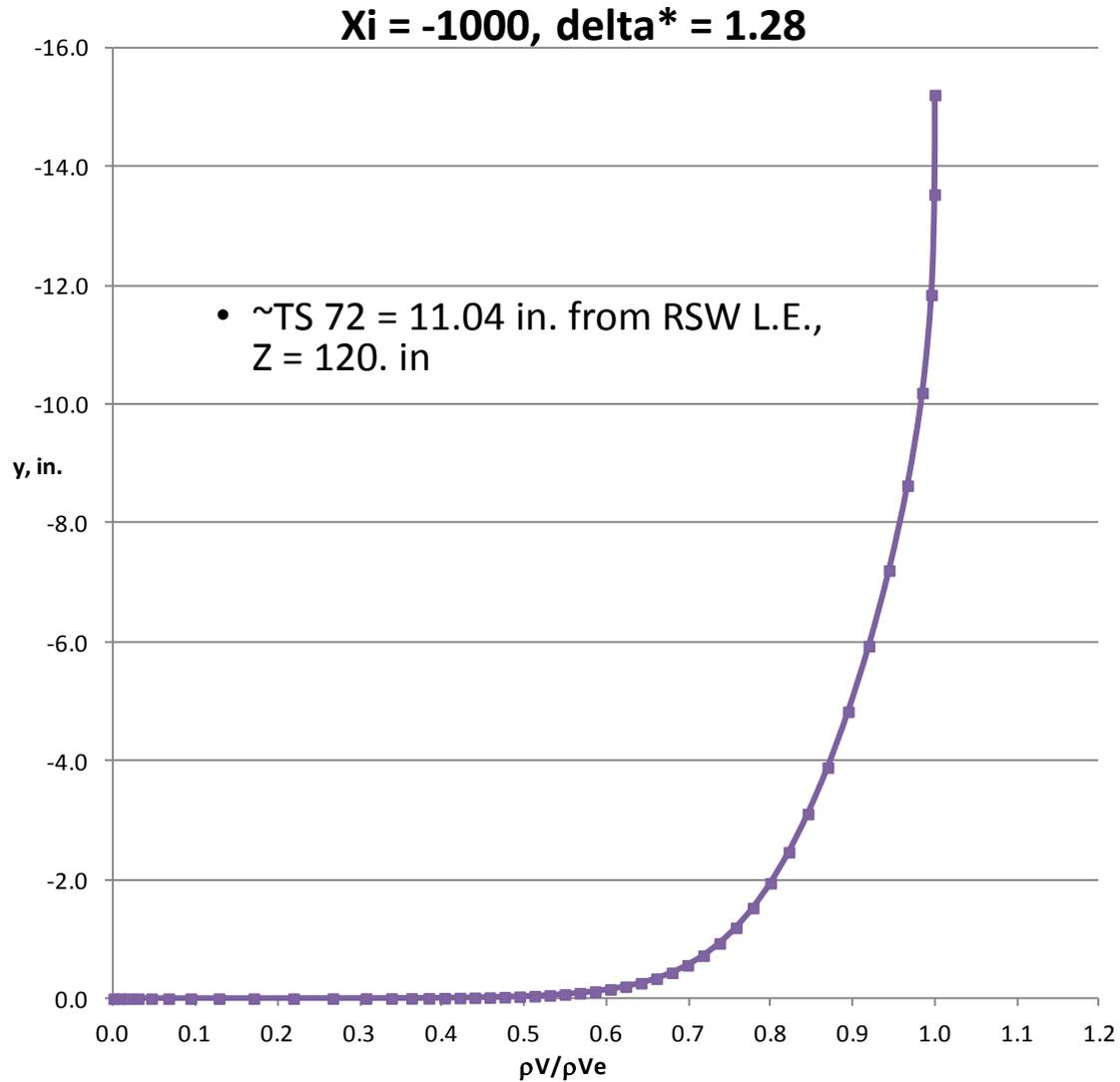


# CFL3D Steady Analysis

- Single Zone C-H Grid
  - 97 x 255 x 65 = 1,560,576 cells
    - spanwise x streamwise x normal
  - Viscous TDT East Wall.
    - No splitter Plate.
  - Forward grid boundary 1000 in. ahead of wing leading edge.
    - BL measured at TDT TS72 = 11.04 in. aft of RSW leading edge, 120 in. above L.E.



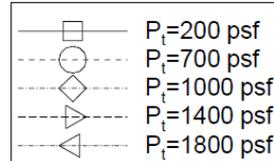
# CFL3D Computed BL



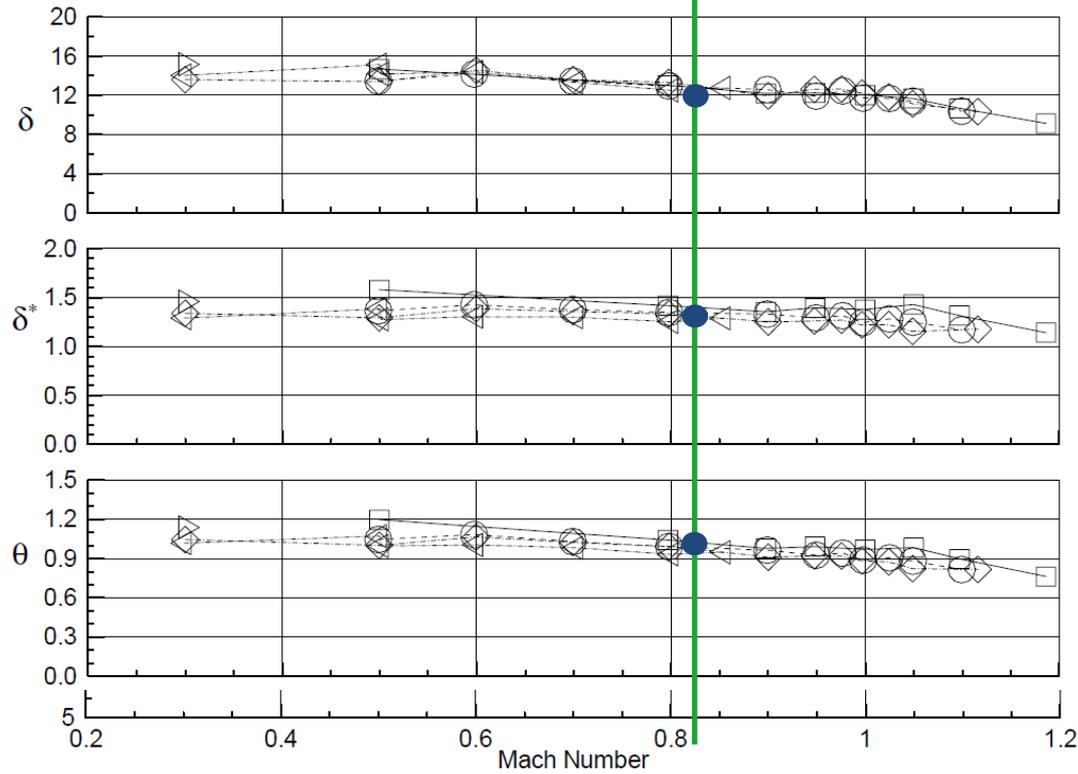


# TDT East Wall Boundary Layer

- Wieseman, C. D. and Bennett, R. M., "Wall Boundary Layer Measurements for the NASA Langley Transonic Dynamics Tunnel," NASA/TM-2007-214867, April, 2007



● CFL3D,  $M = 0.825$ ,  $\alpha = 2.00^\circ$ ,  
 $X_i = -1000$  in.

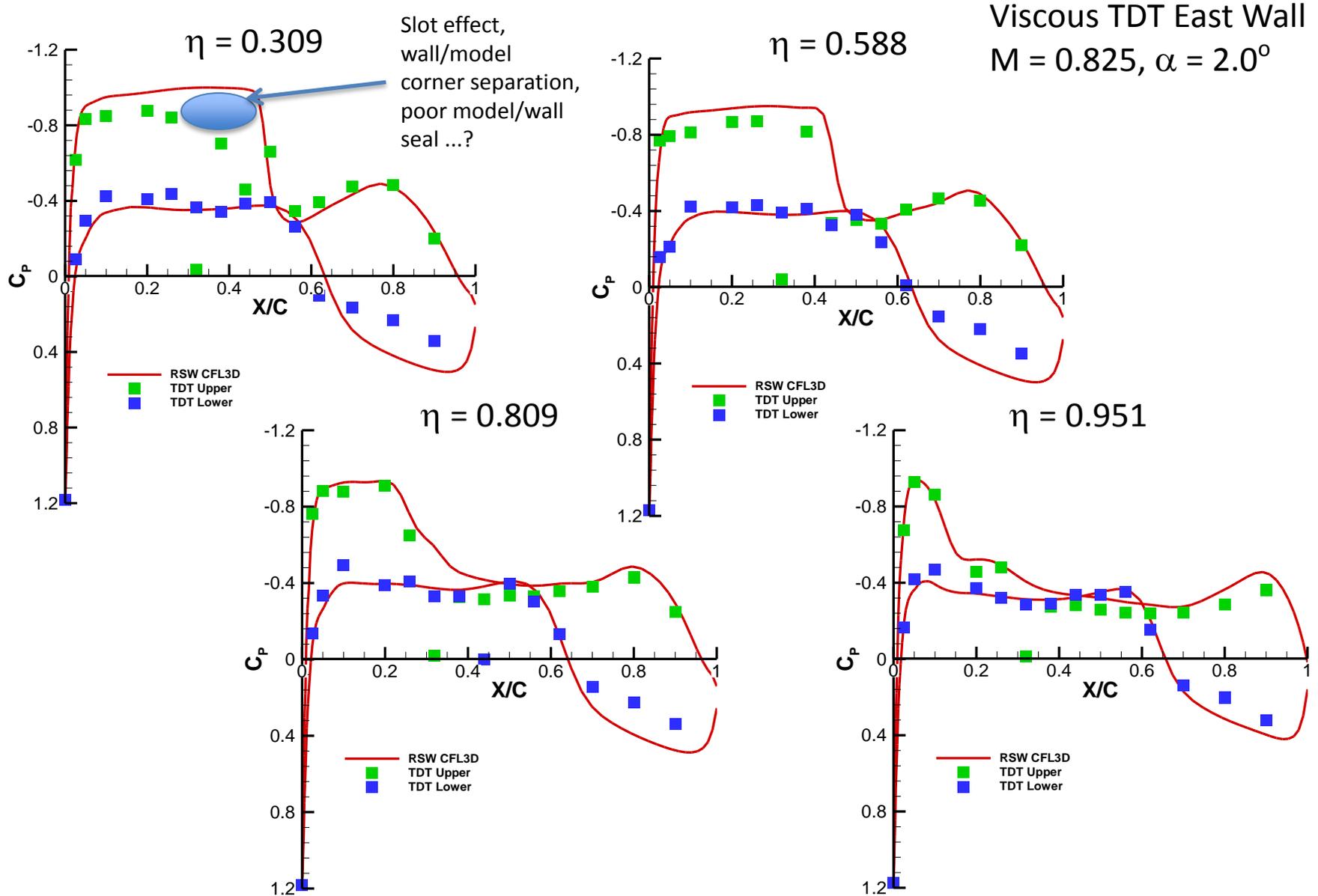


a) East wall rake

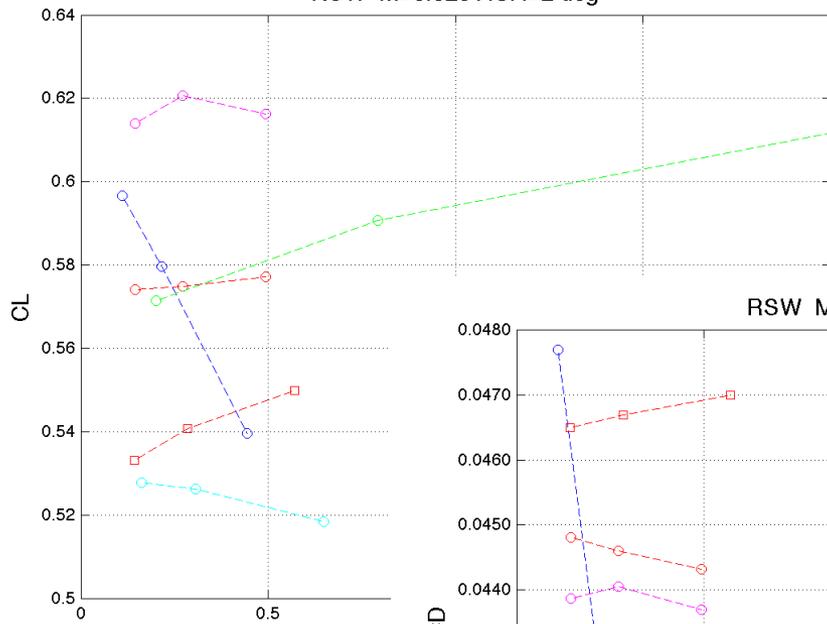
Figure 17. Boundary layer parameters for R-134a, all slots open, TS 72, standard flap settings.



# RSW CFL3D Calculation

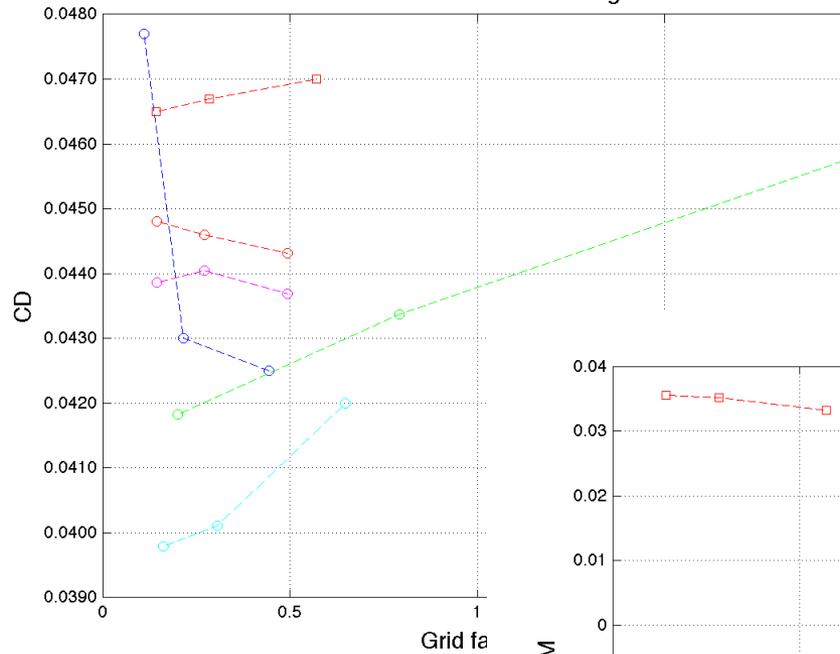


RSW M=0.826 AOA=2 deg

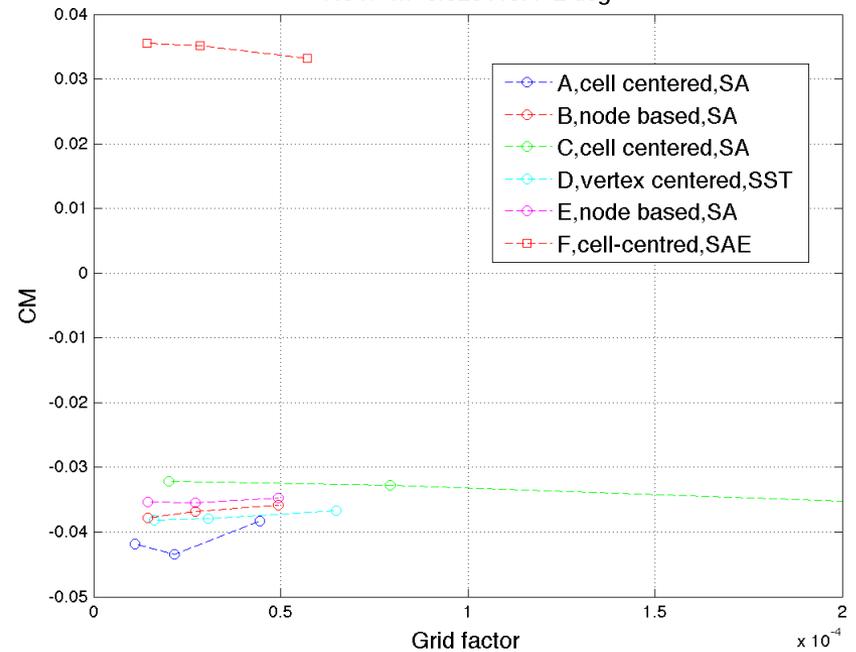


Note: not all analyses utilize the same Normalization parameters and moment reference center. These issues will need to be sorted out in the post-workshop corrections

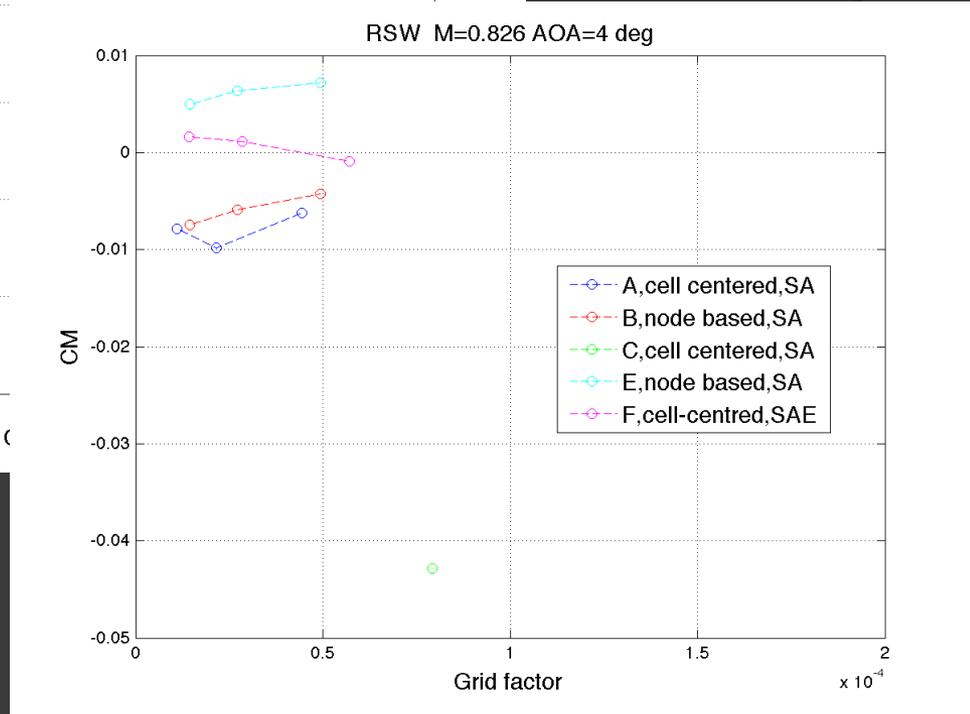
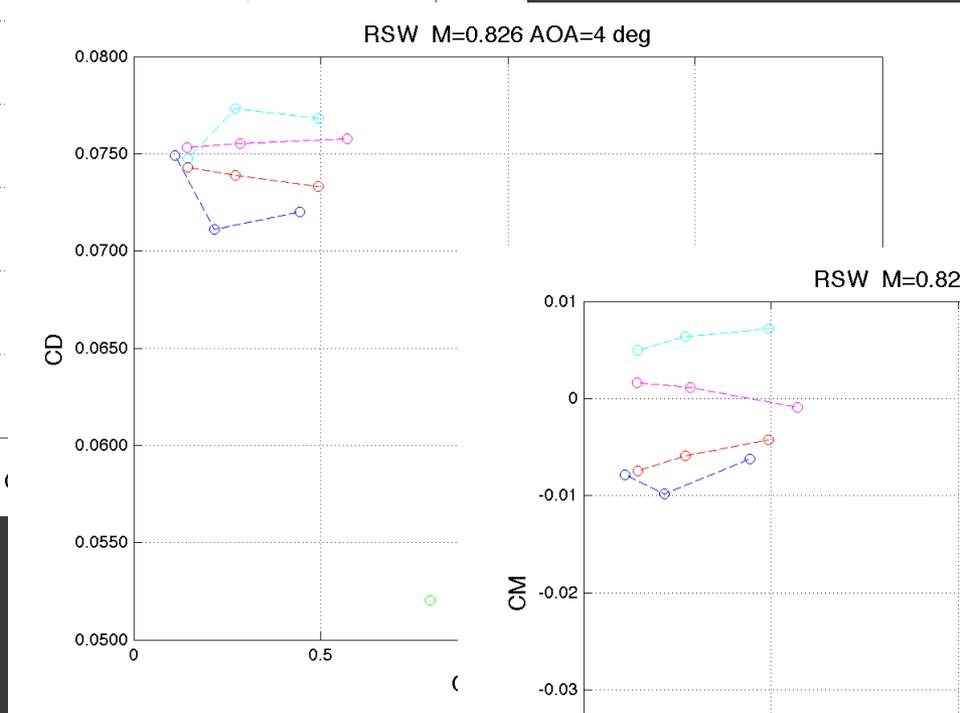
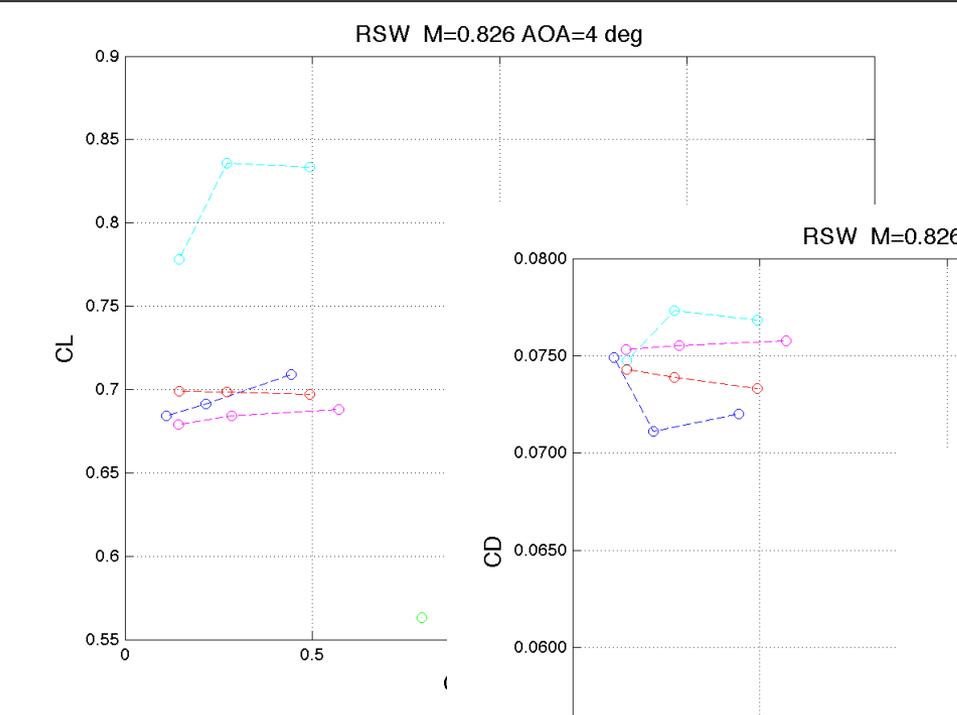
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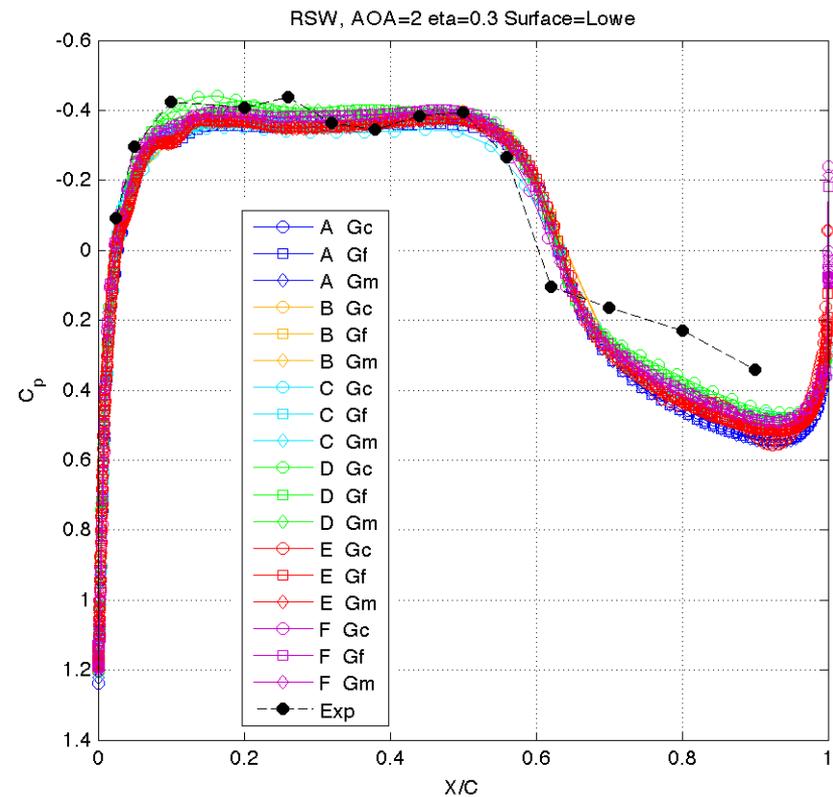
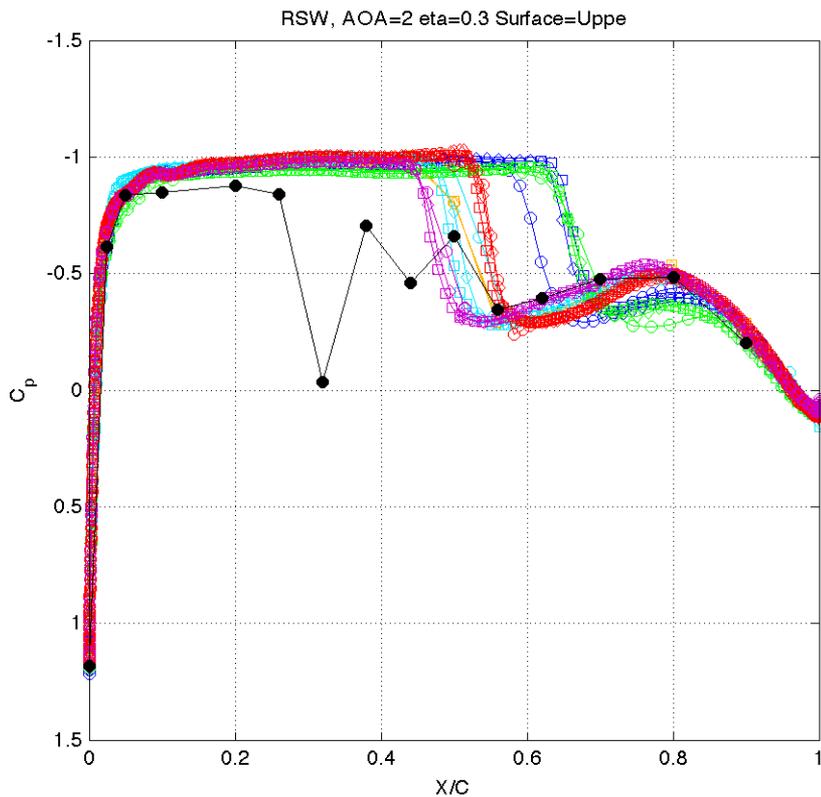


# STEADY

$$M = 0.825, \alpha = 2^\circ$$

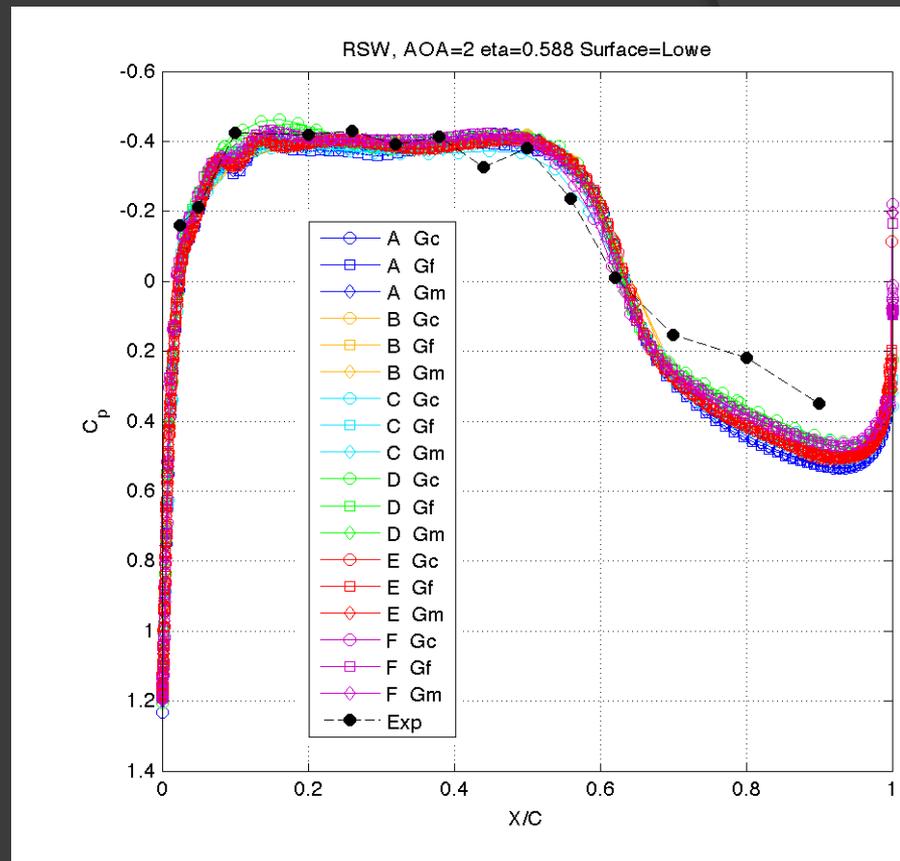
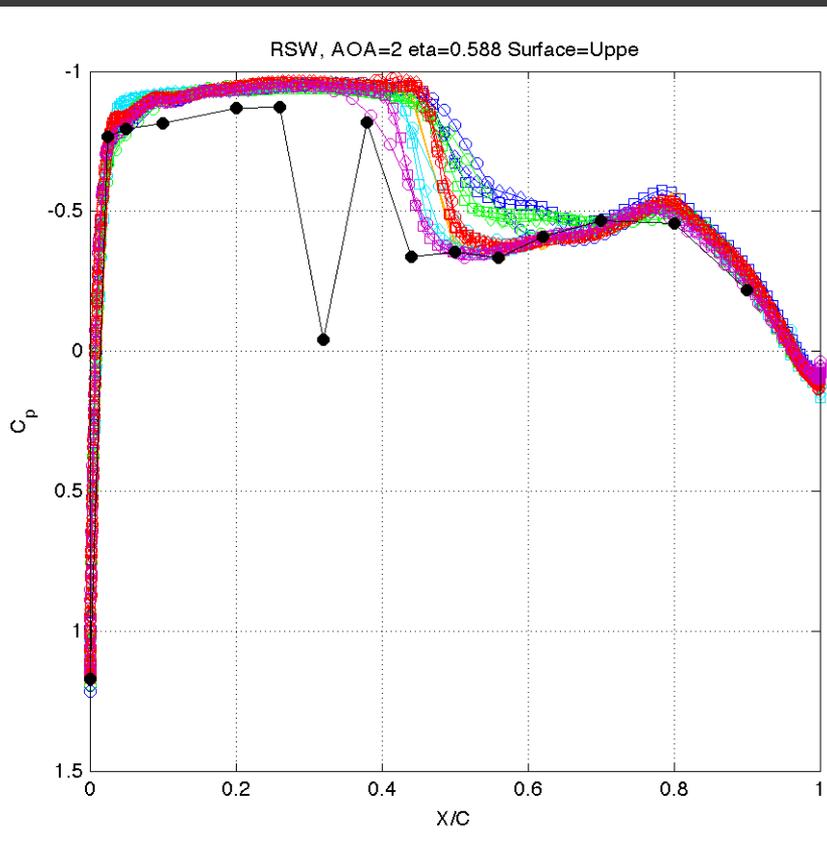
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# Upper $\eta = 0.309$ Lower



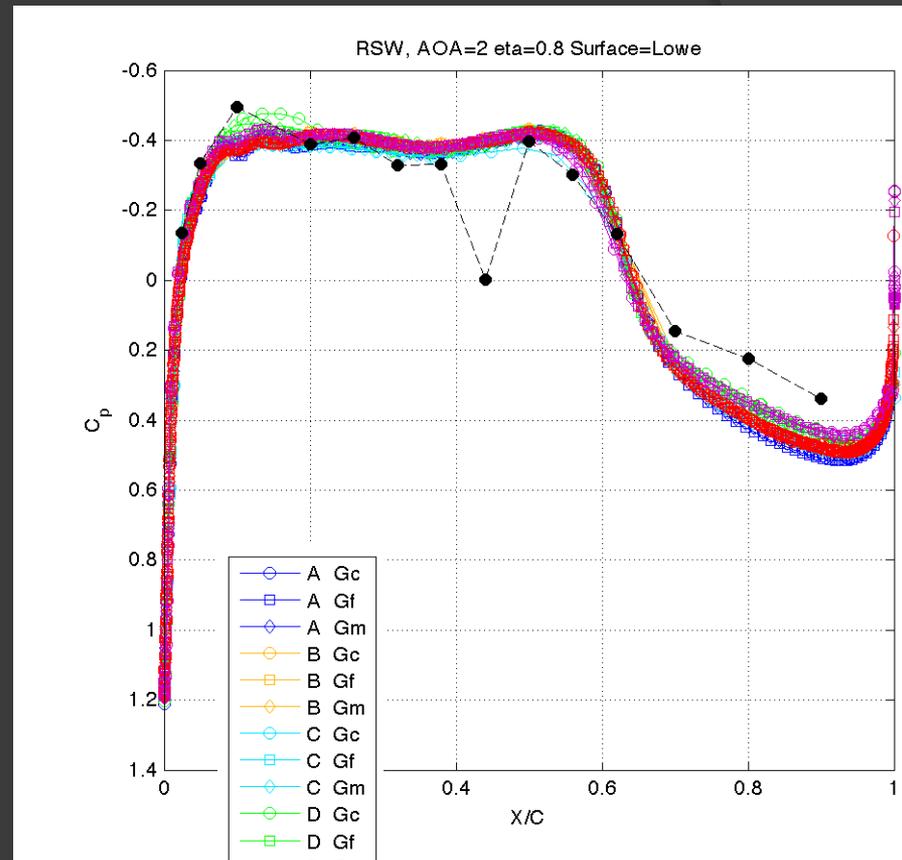
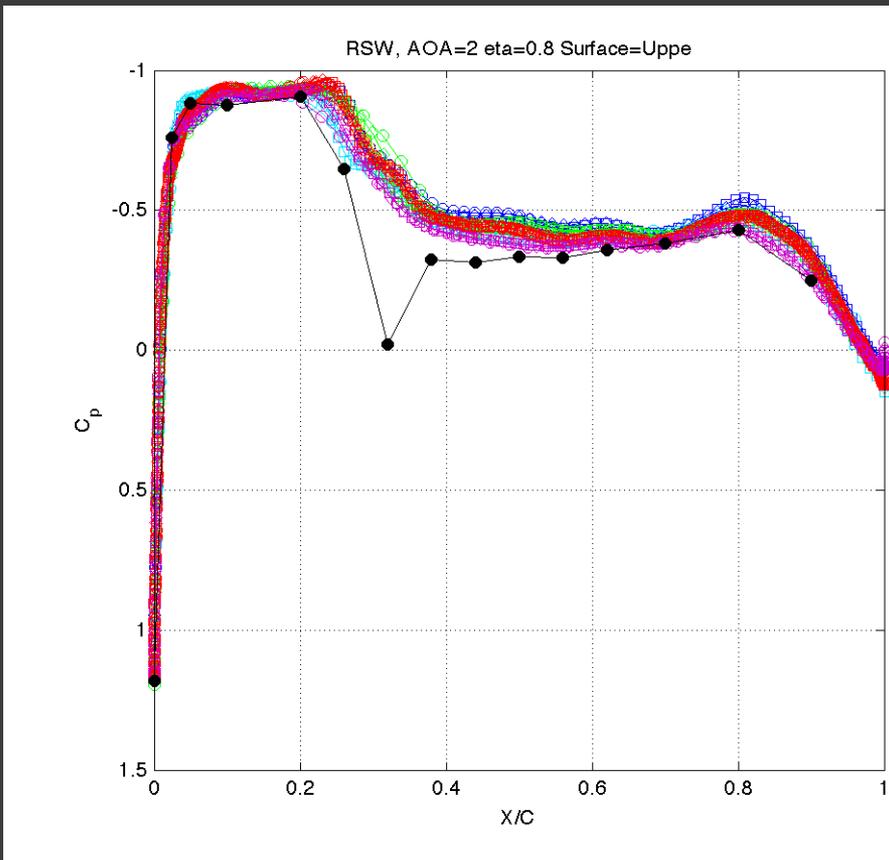
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# Upper $\eta = 0.588$ Lower



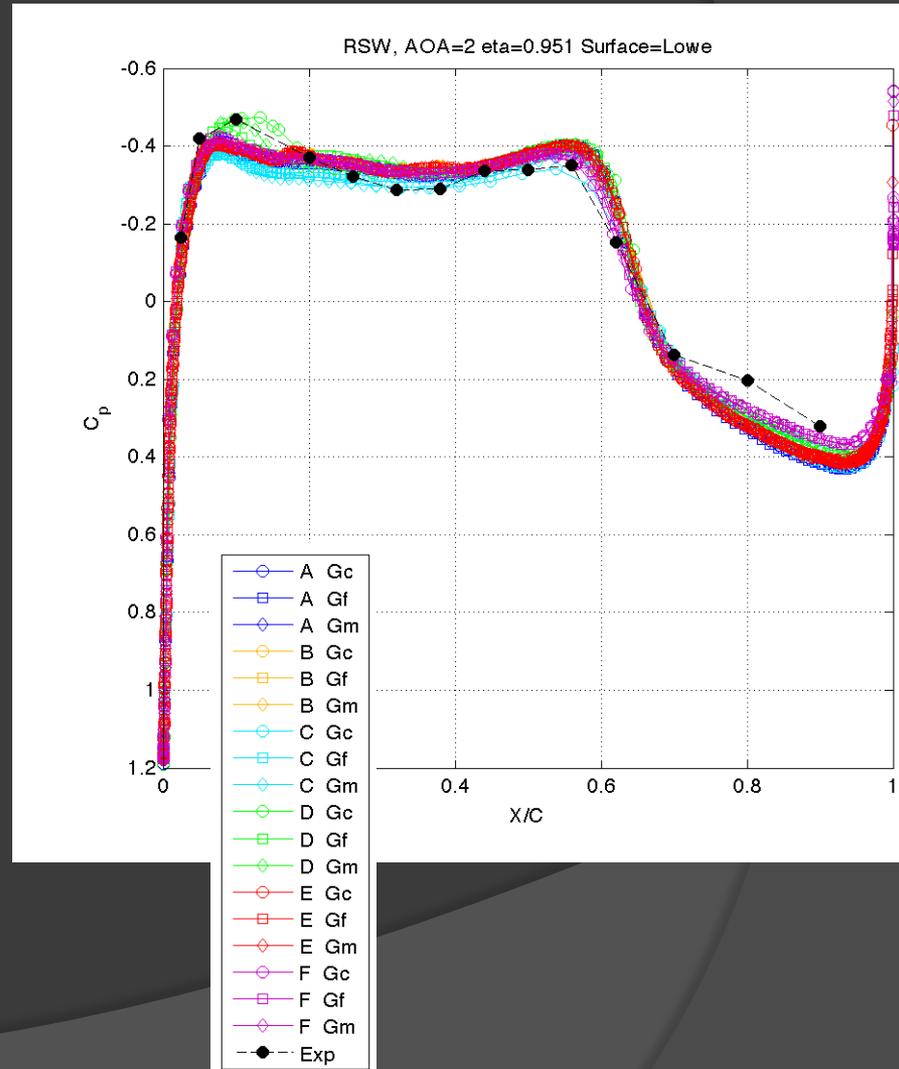
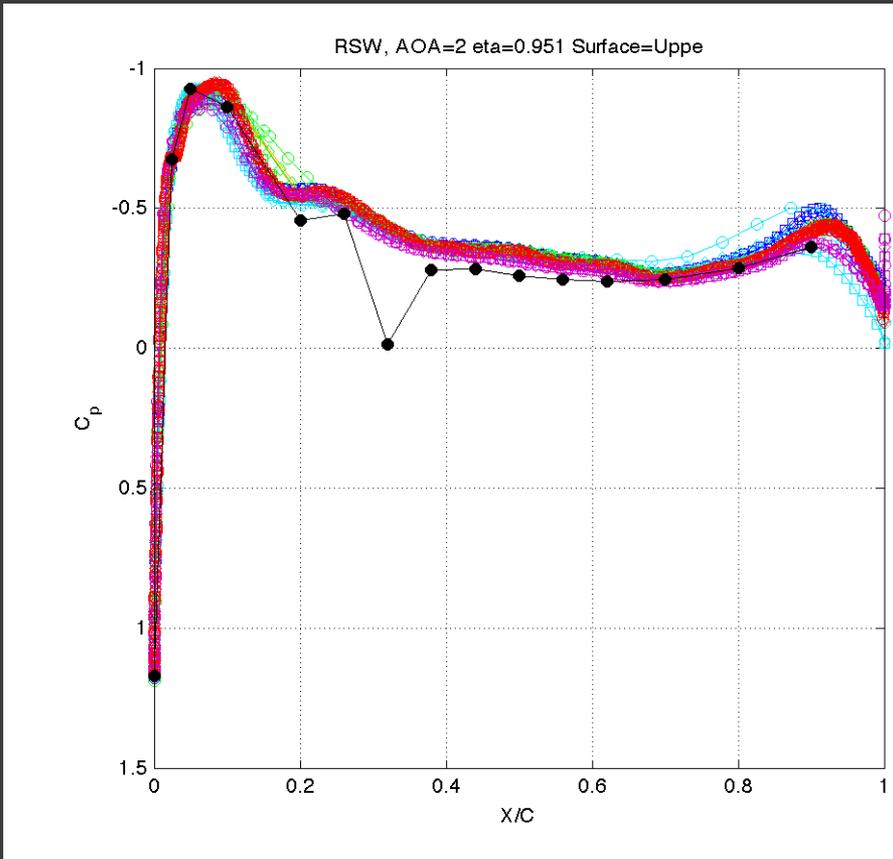
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# Upper $\eta = 0.809$ Lower



- A Gc
- A Gf
- ◇— A Gm
- B Gc
- B Gf
- ◇— B Gm
- C Gc
- C Gf
- ◇— C Gm
- D Gc
- D Gf
- ◇— D Gm
- E Gc
- E Gf
- ◇— E Gm
- F Gc
- F Gf
- ◇— F Gm
- Exp

# Upper $\eta = 0.951$ Lower



# STEADY

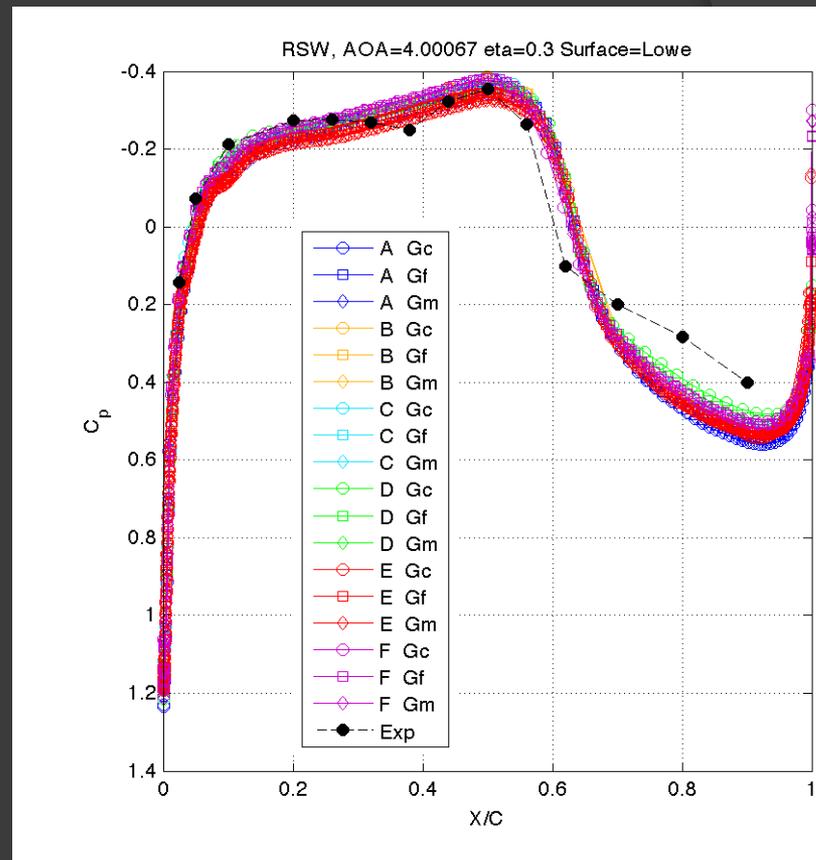
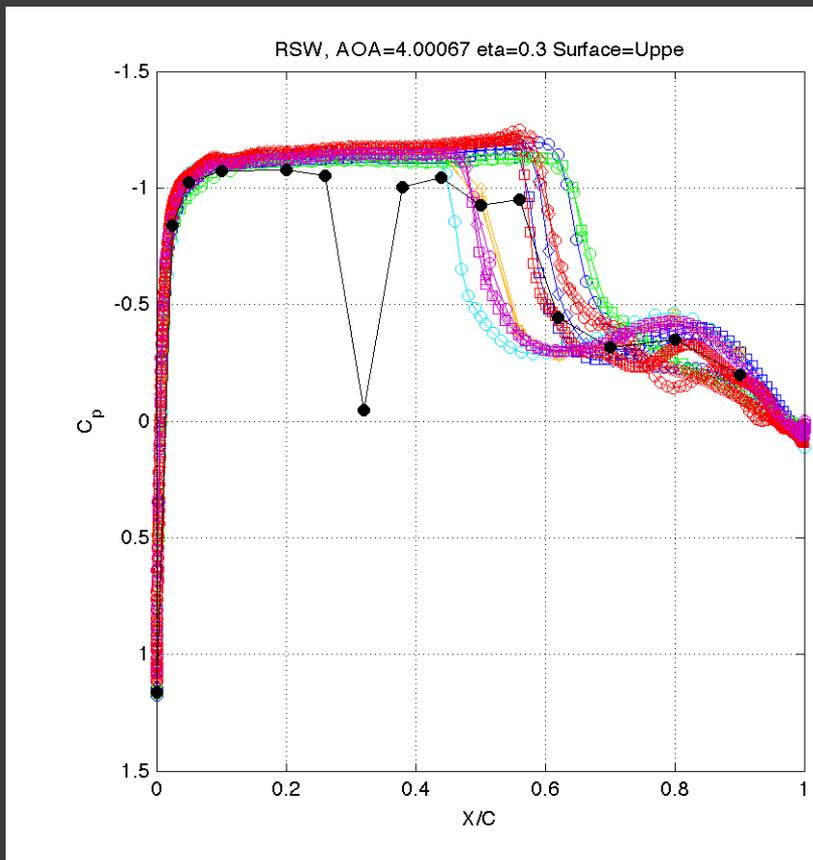
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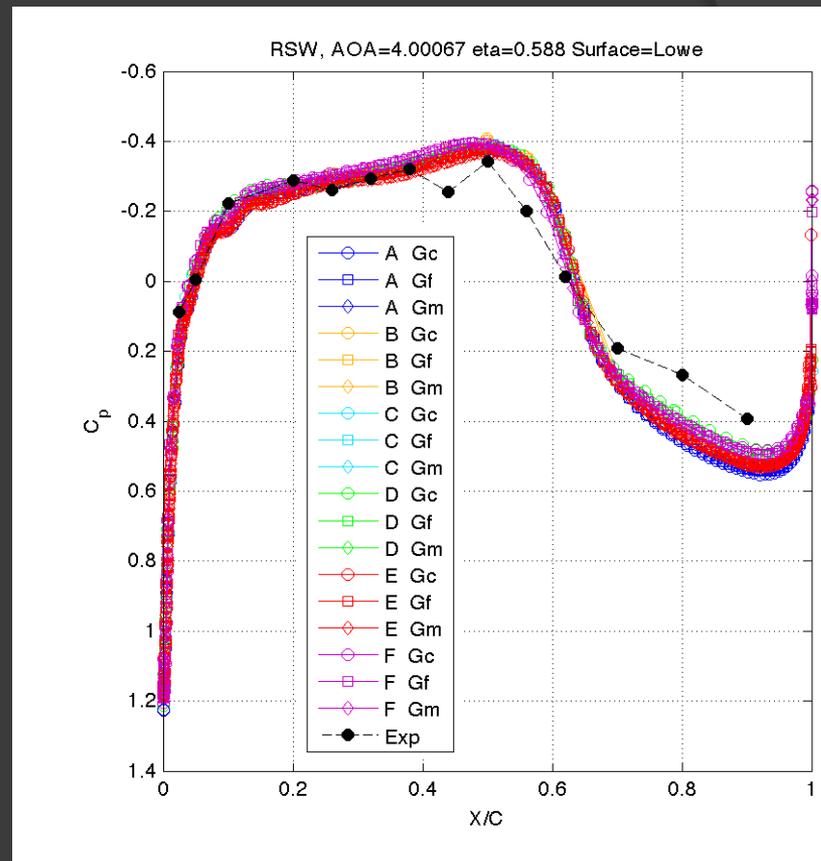
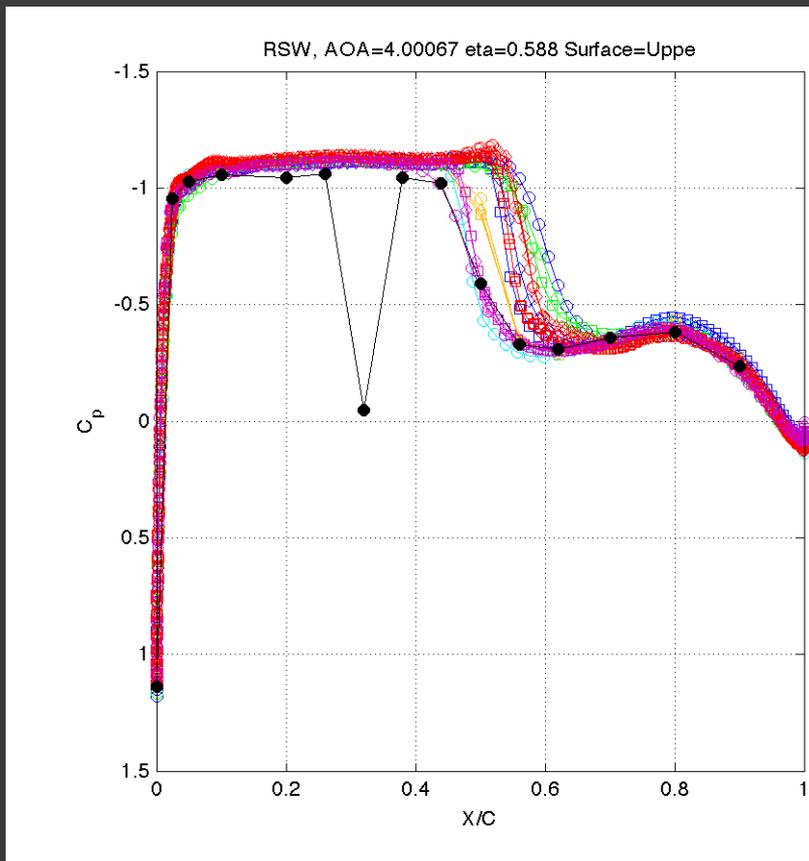
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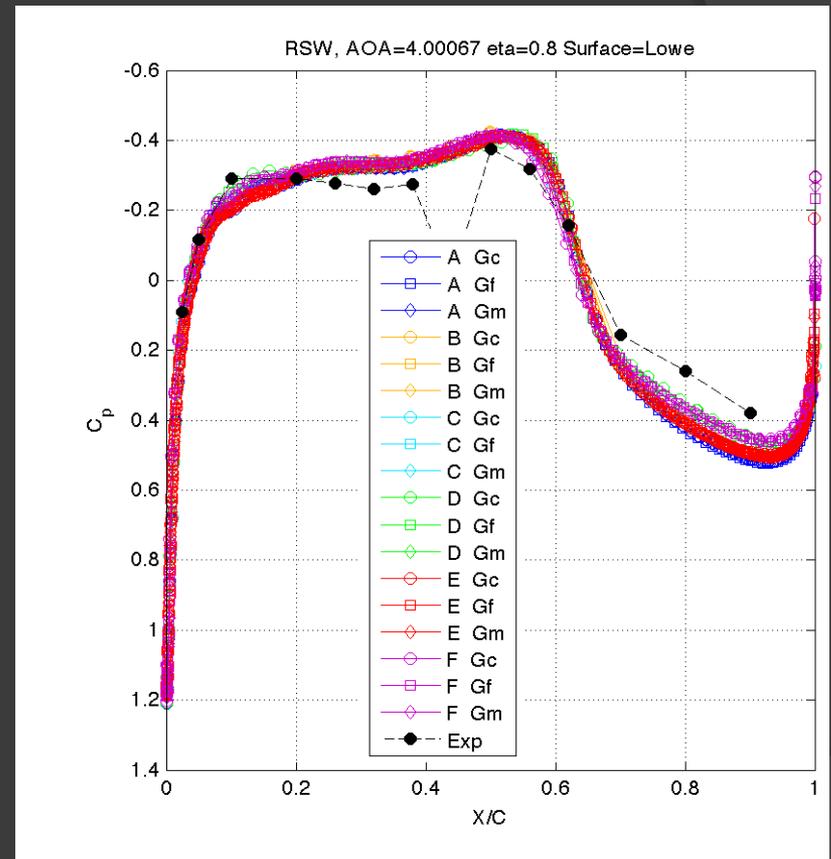
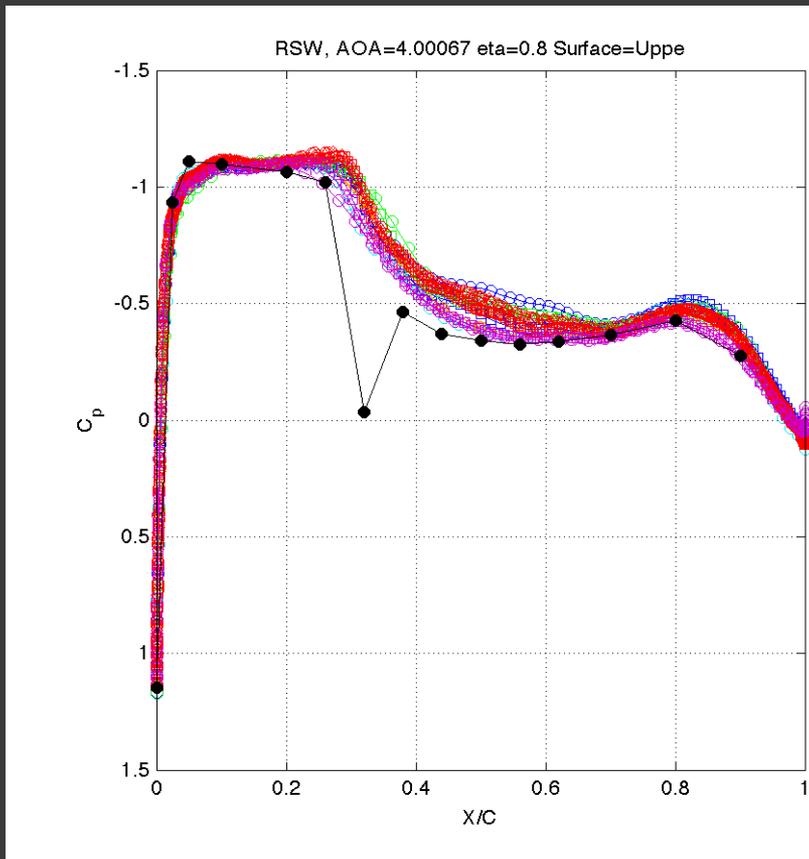
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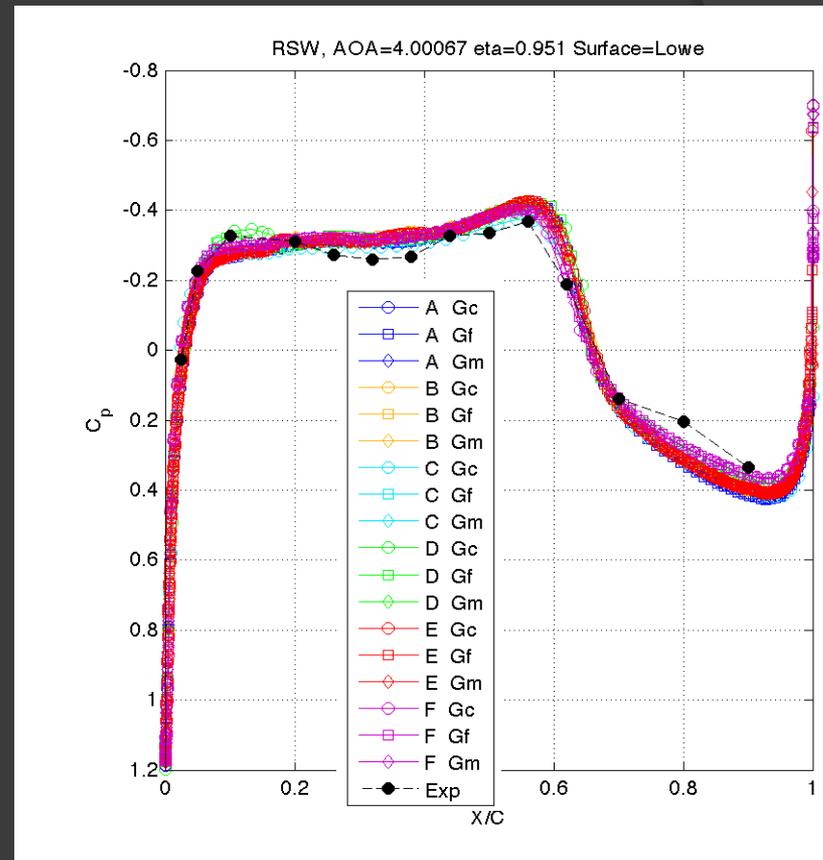
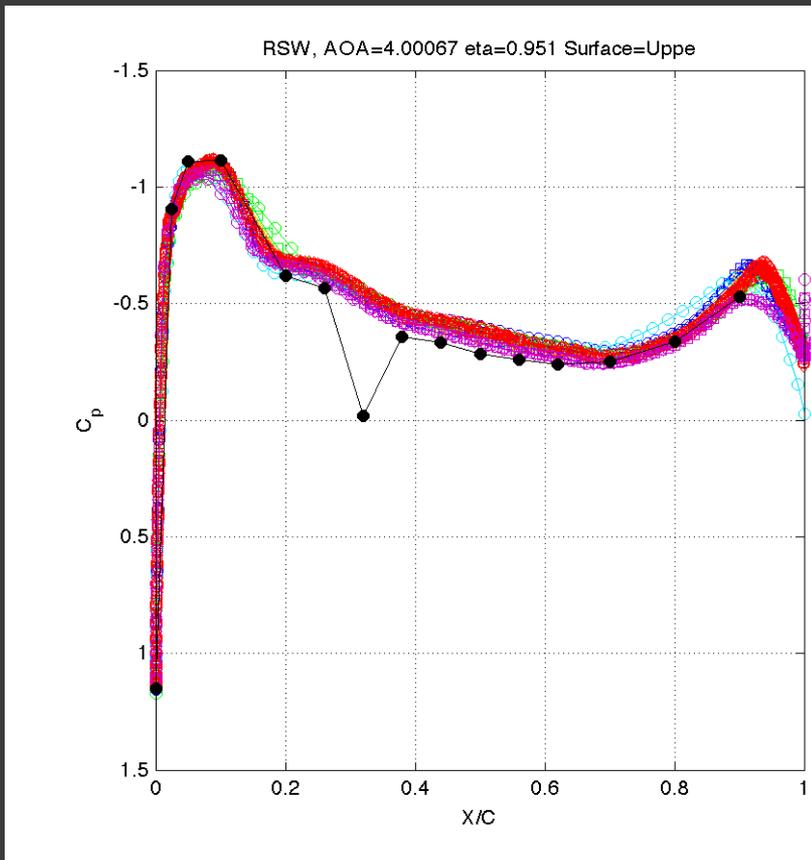


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# UNSTEADY

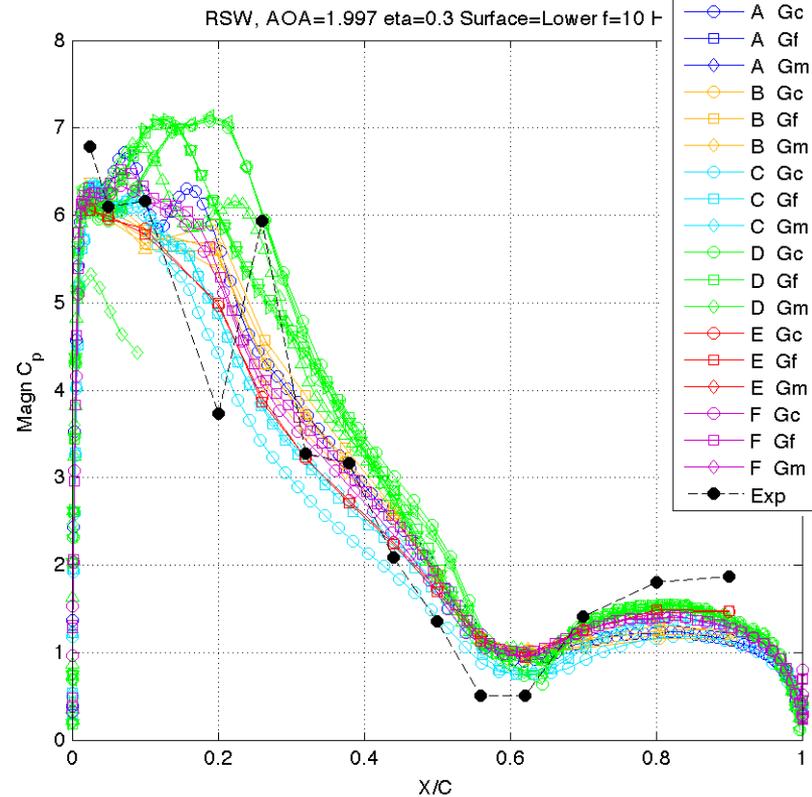
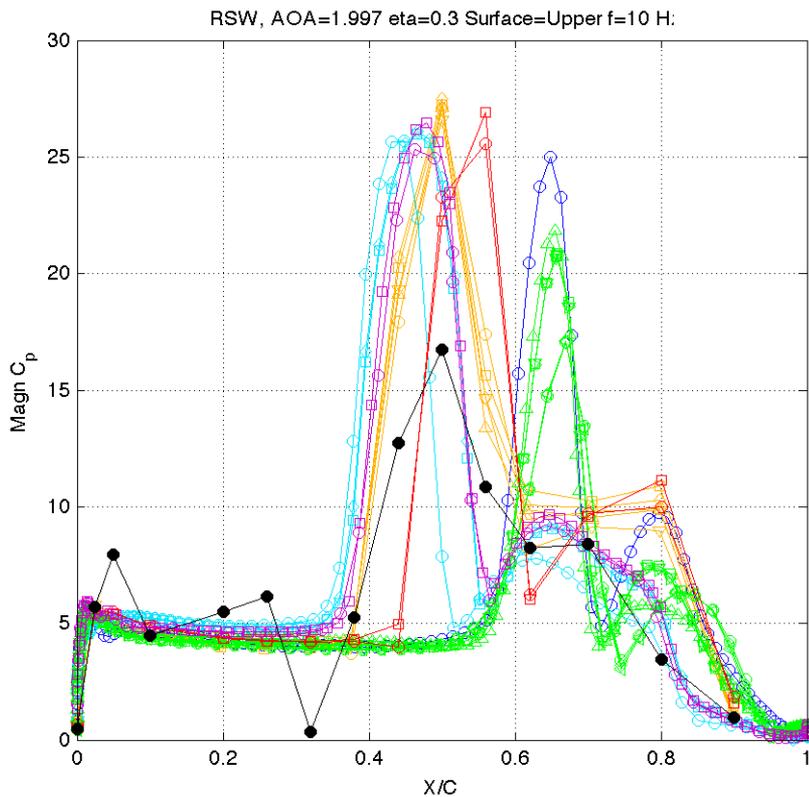
$$M = 0.825, \alpha = 2^\circ, \theta = 1^\circ, f = 10 \text{ Hz.}$$

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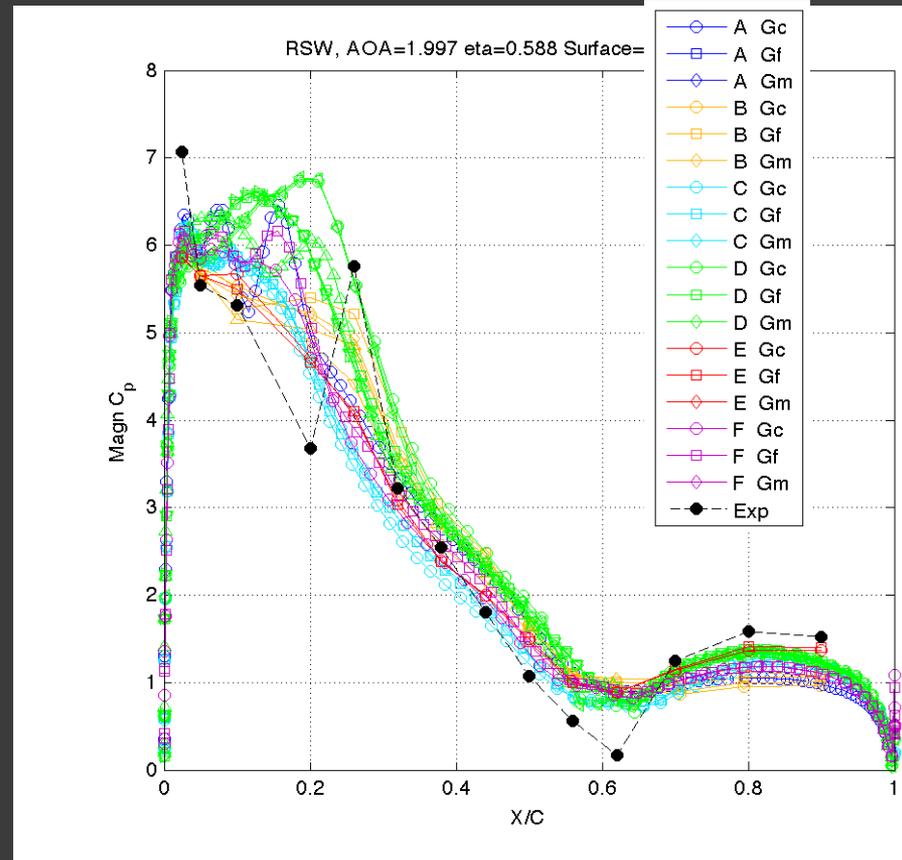
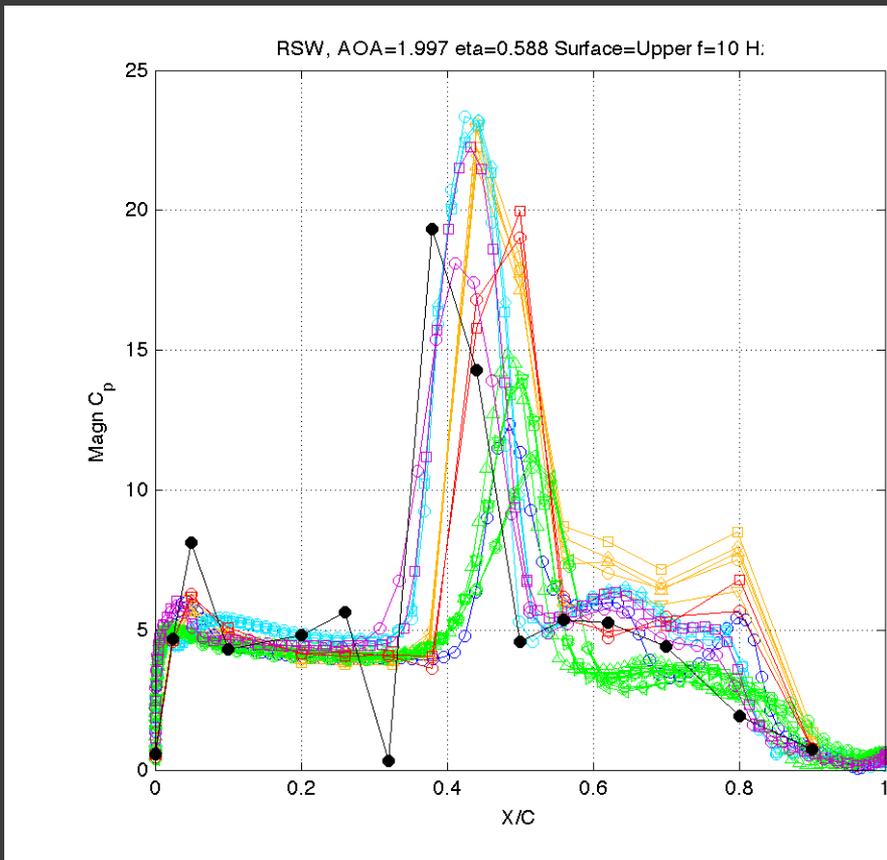
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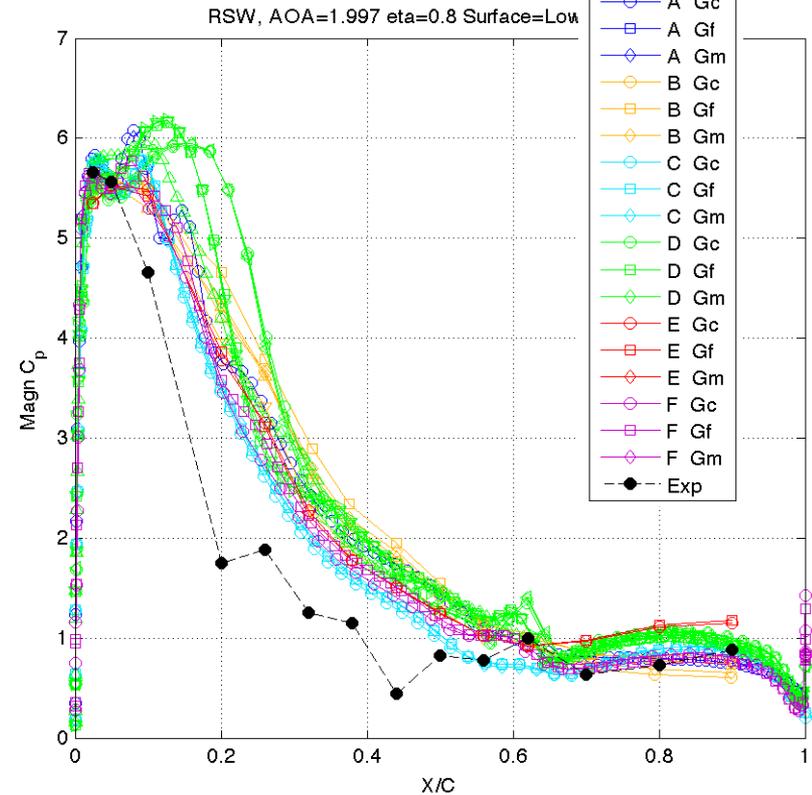
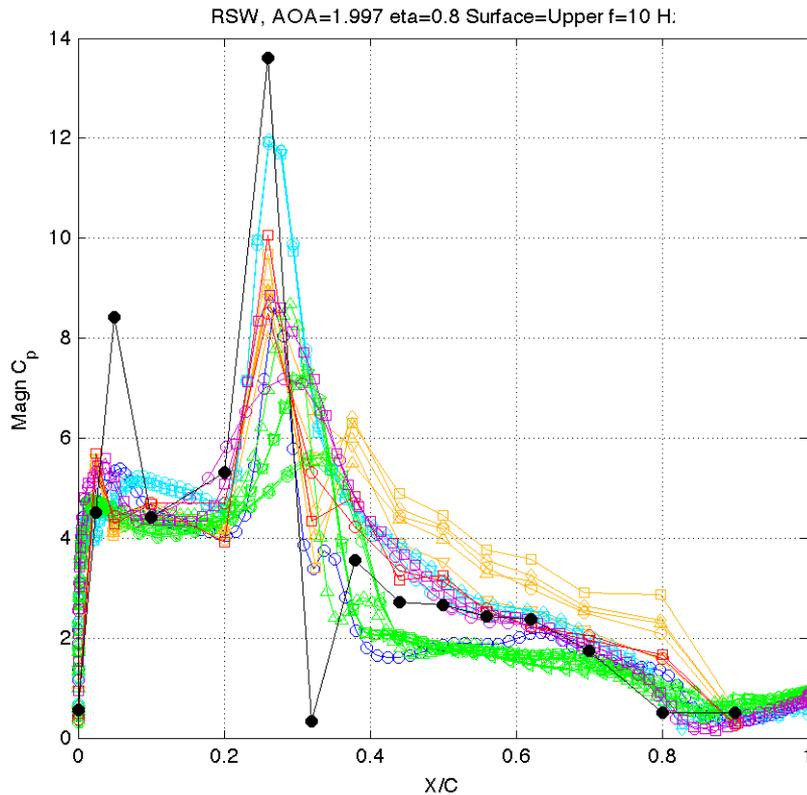
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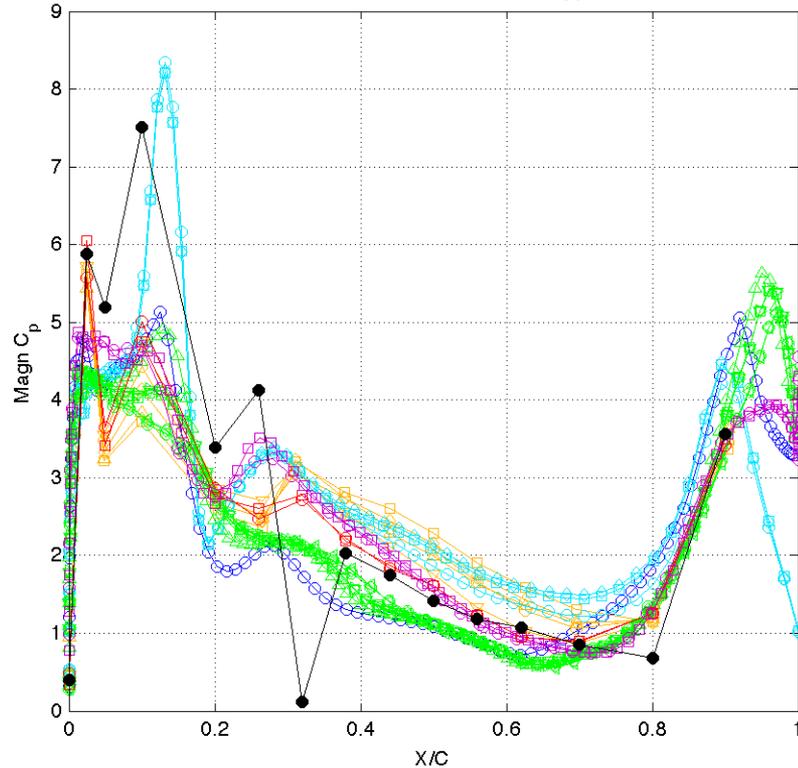
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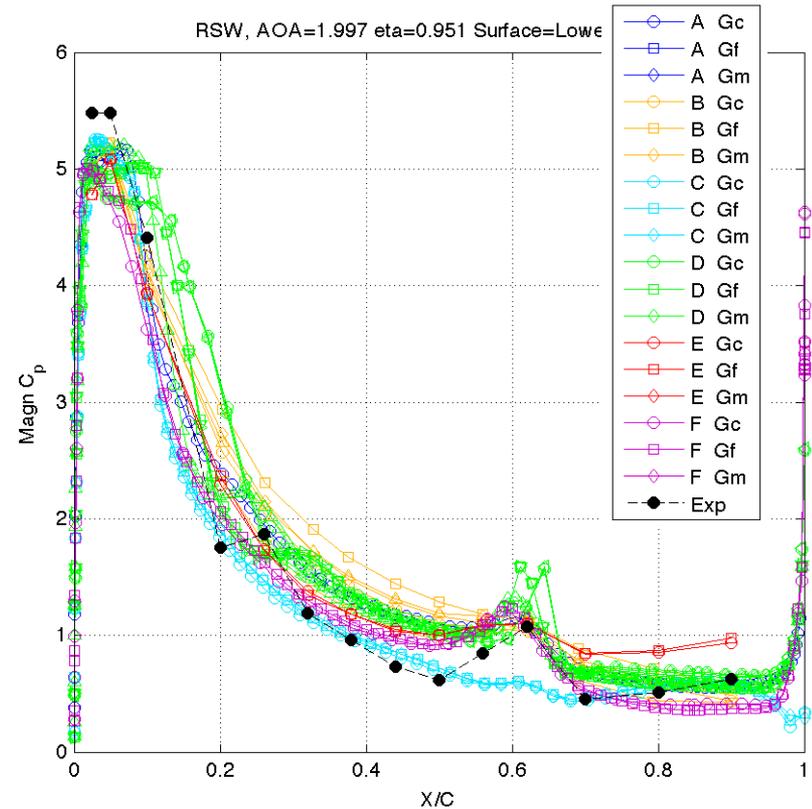
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# Upper $\eta = 0.951$ Lower

RSW, AOA=1.997 eta=0.951 Surface=Upper f=10 Hz:

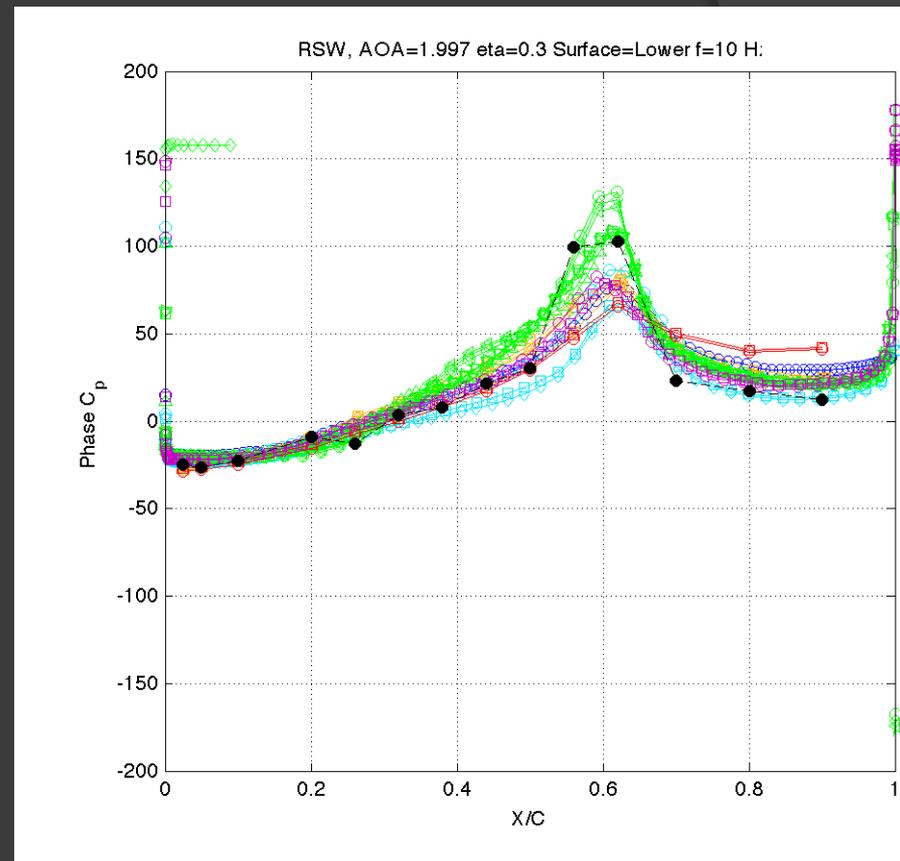
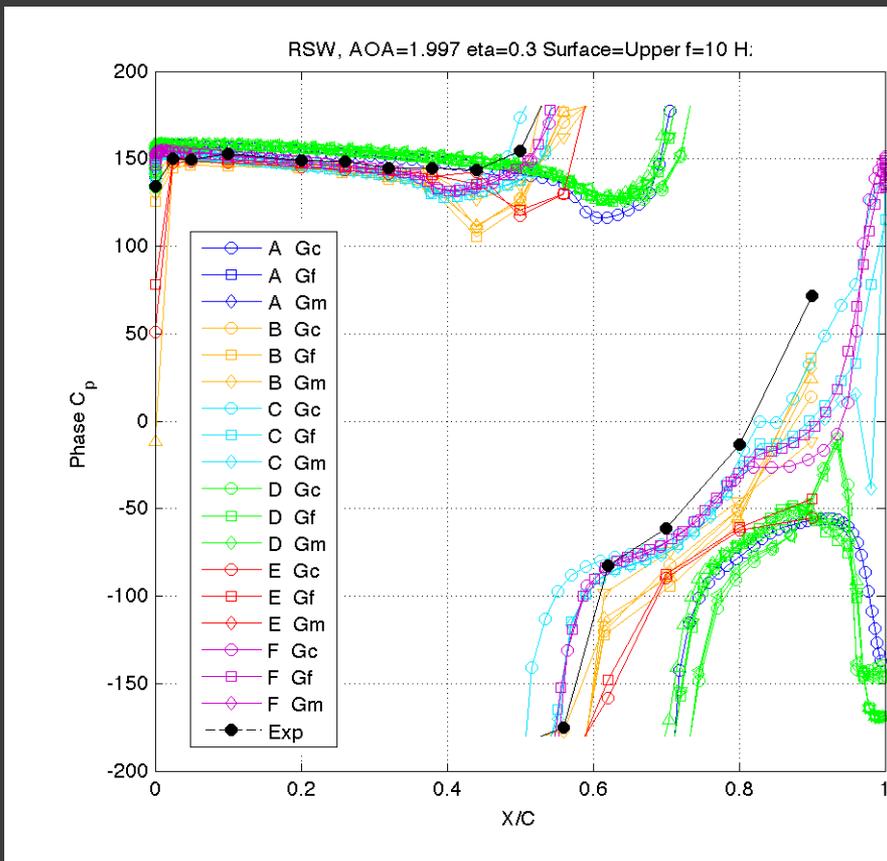


RSW, AOA=1.997 eta=0.951 Surface=Lower



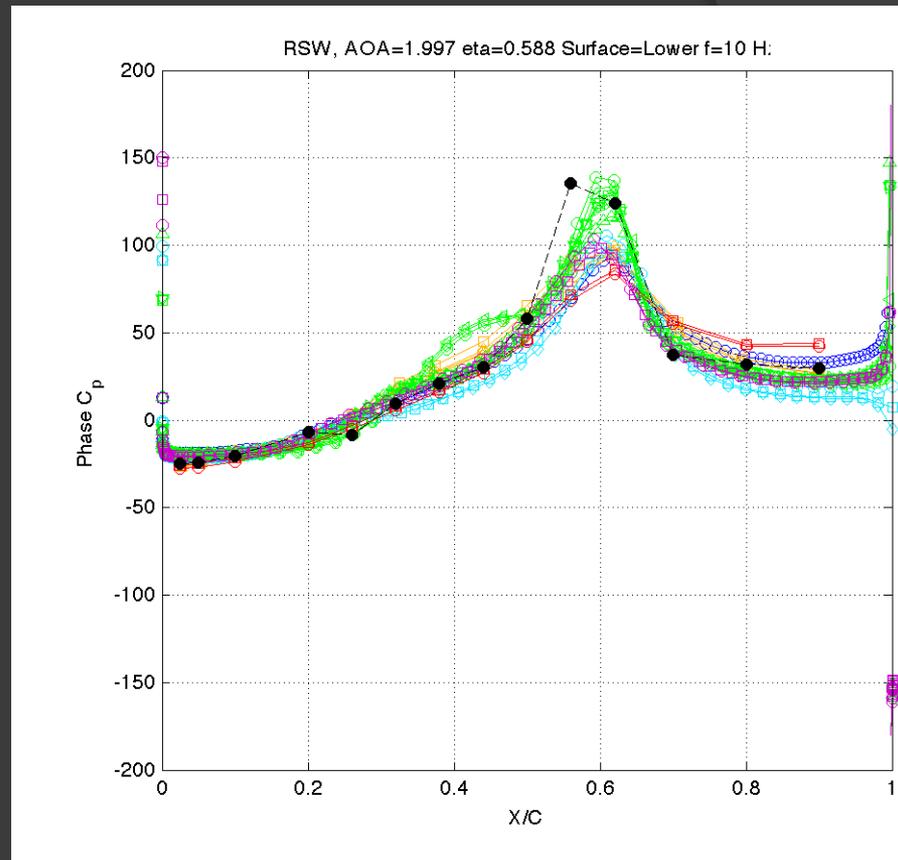
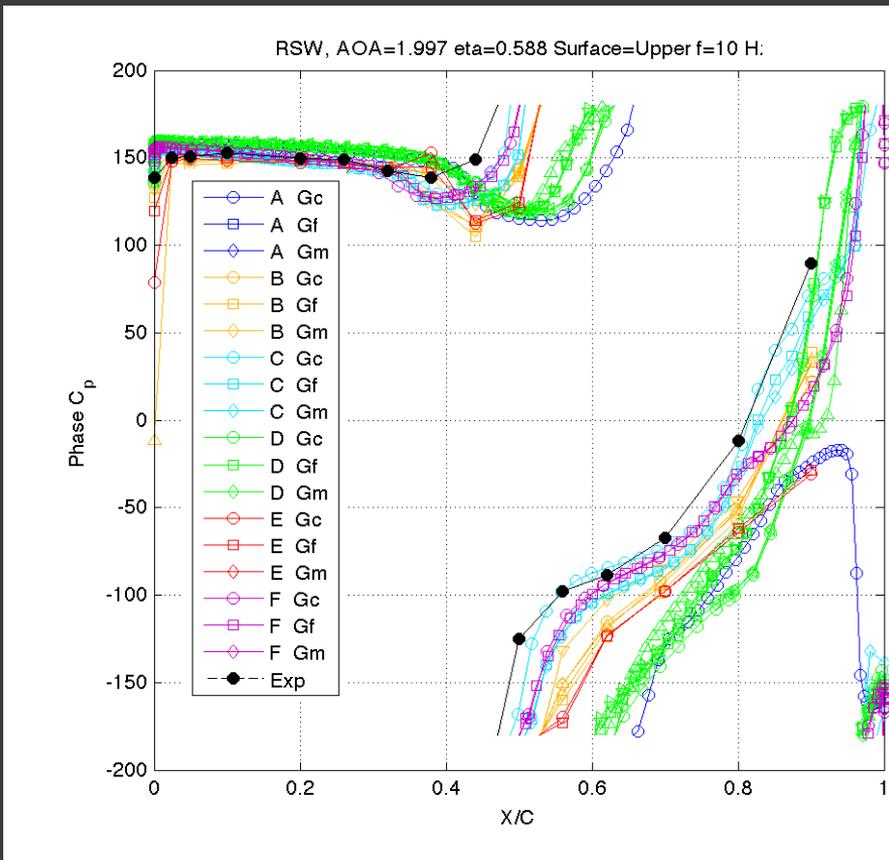
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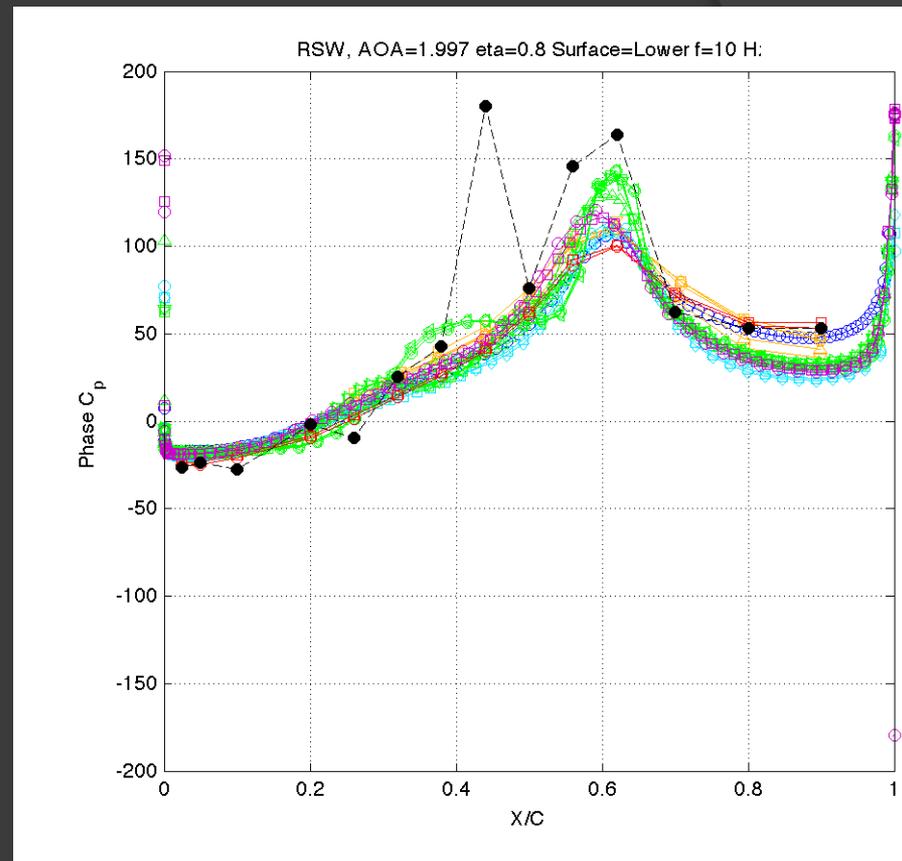
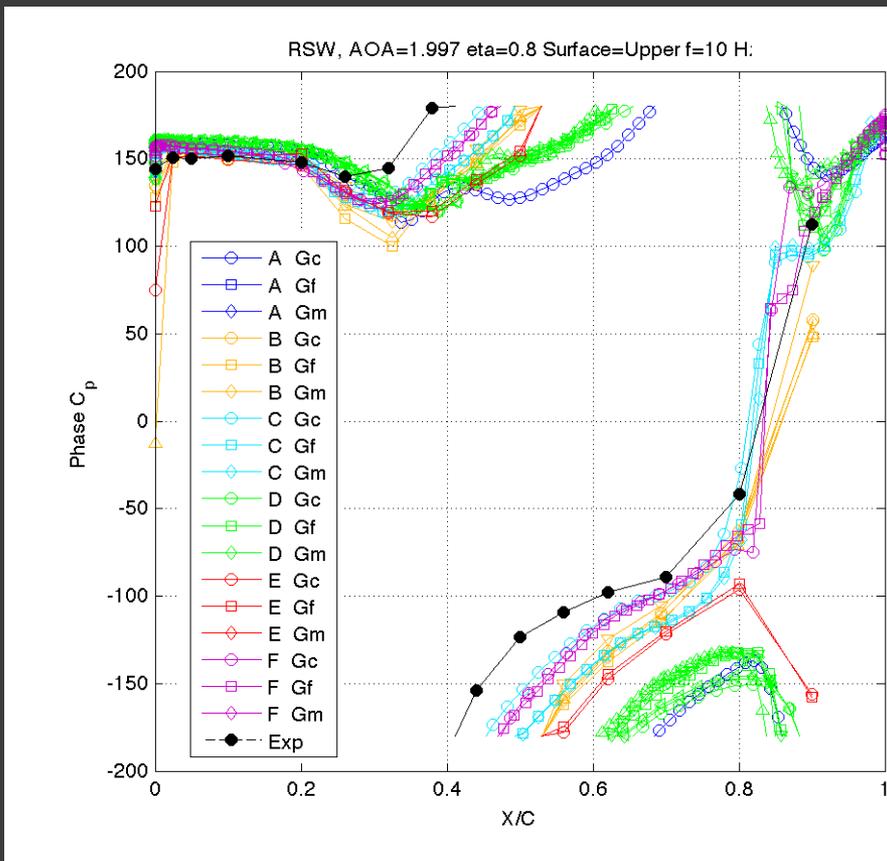
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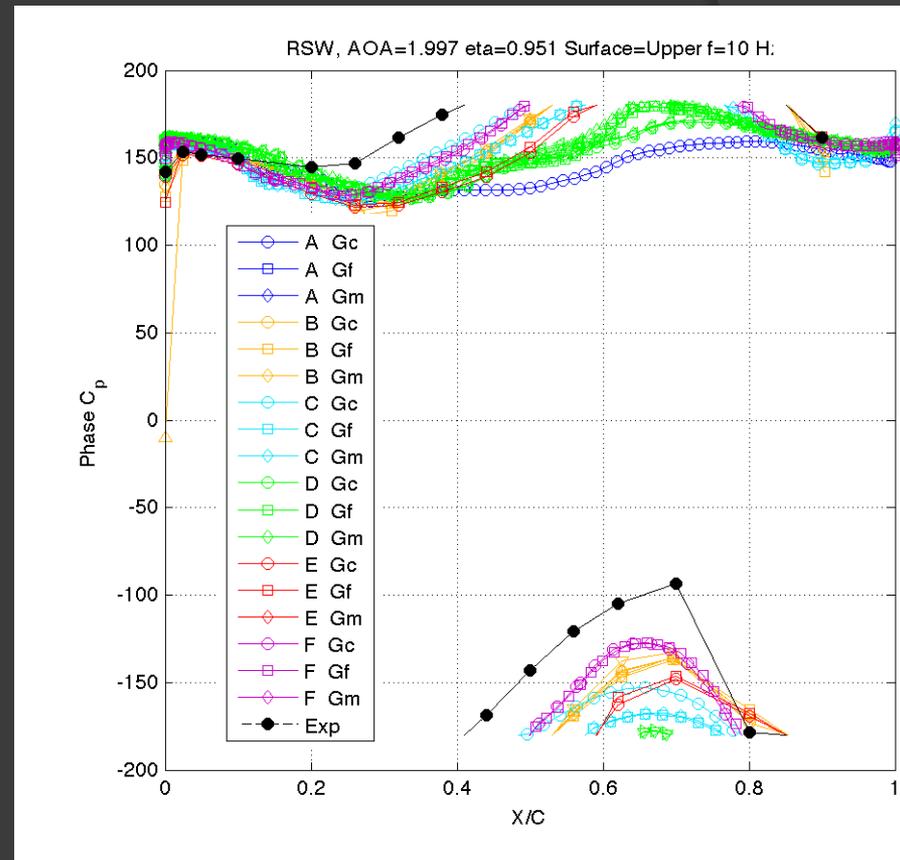
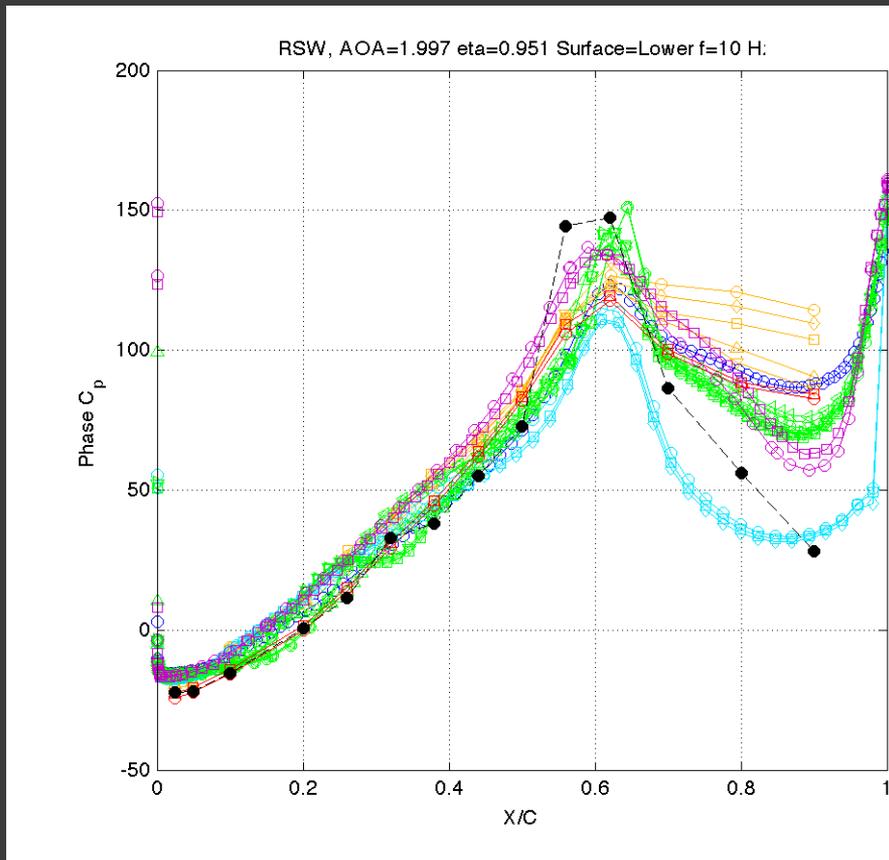
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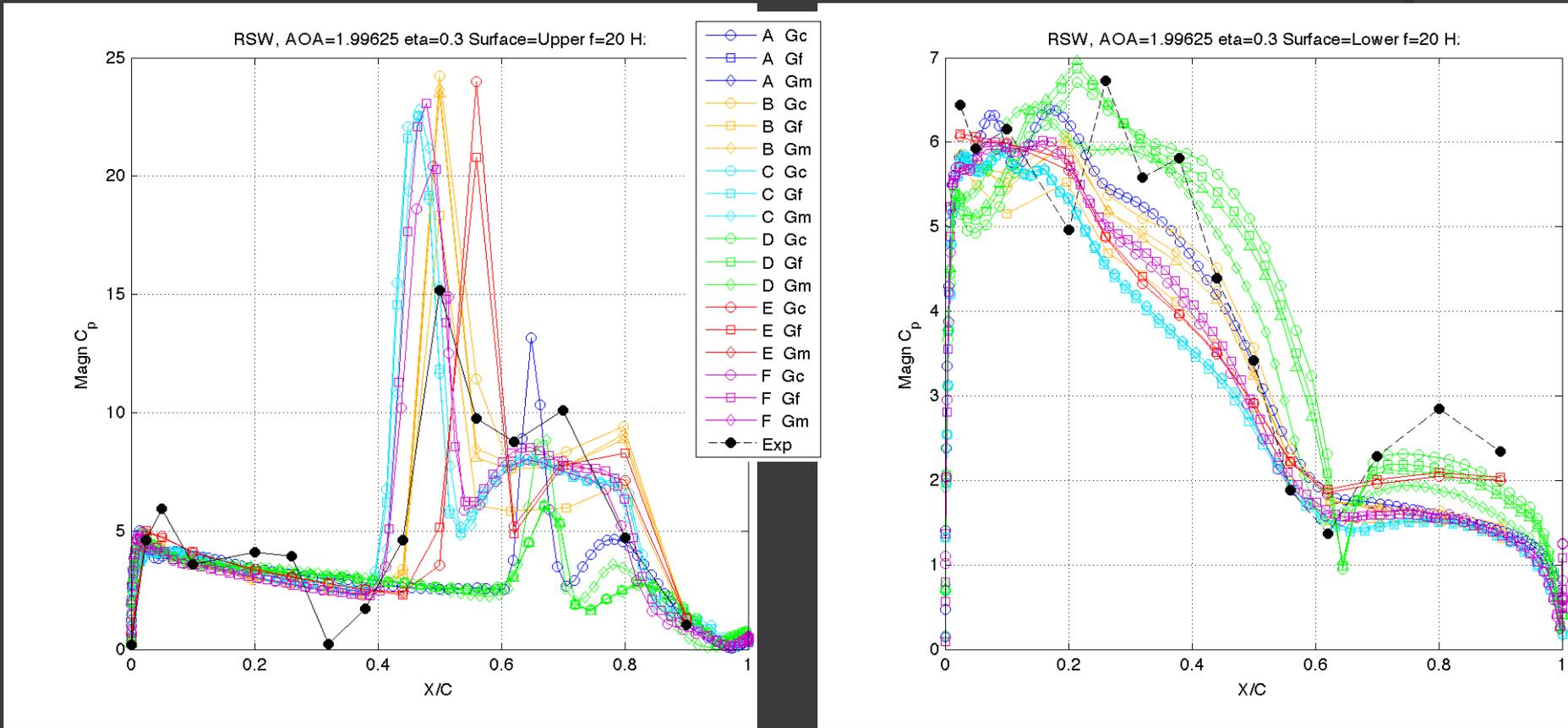
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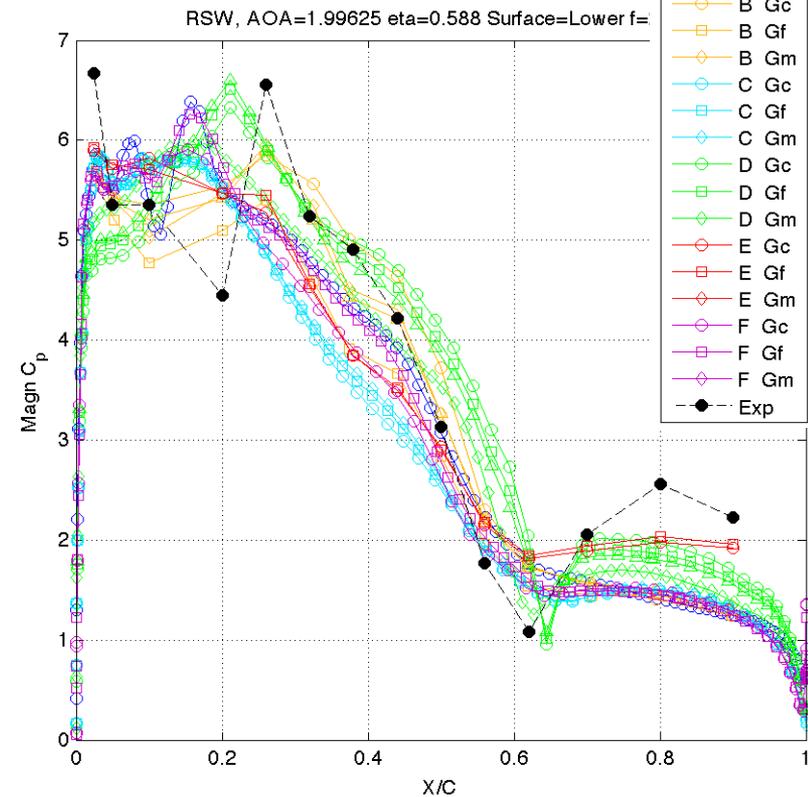
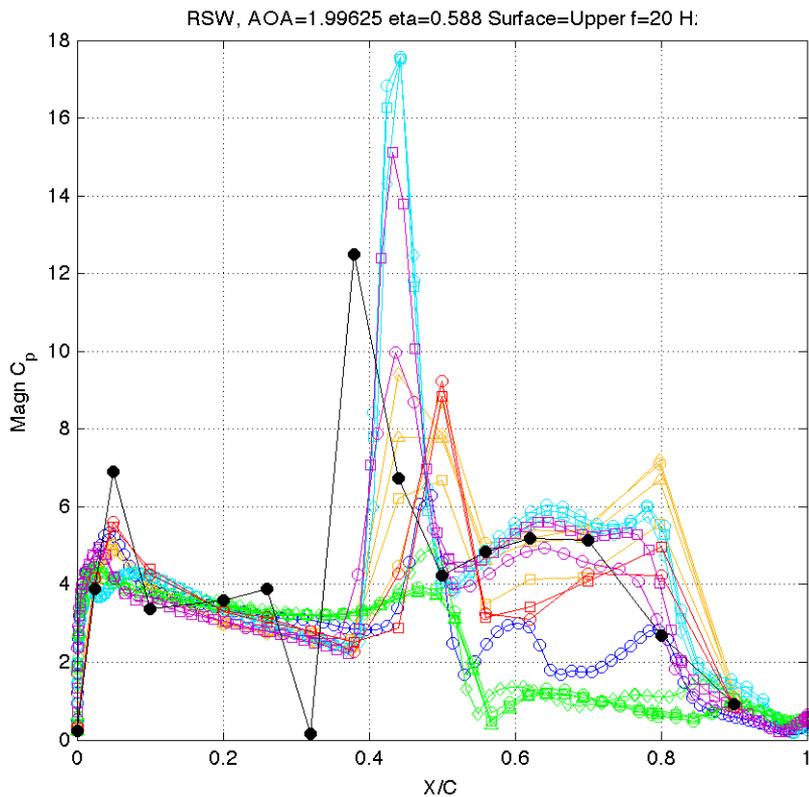
UNSTEADY  $f=20$  Hz

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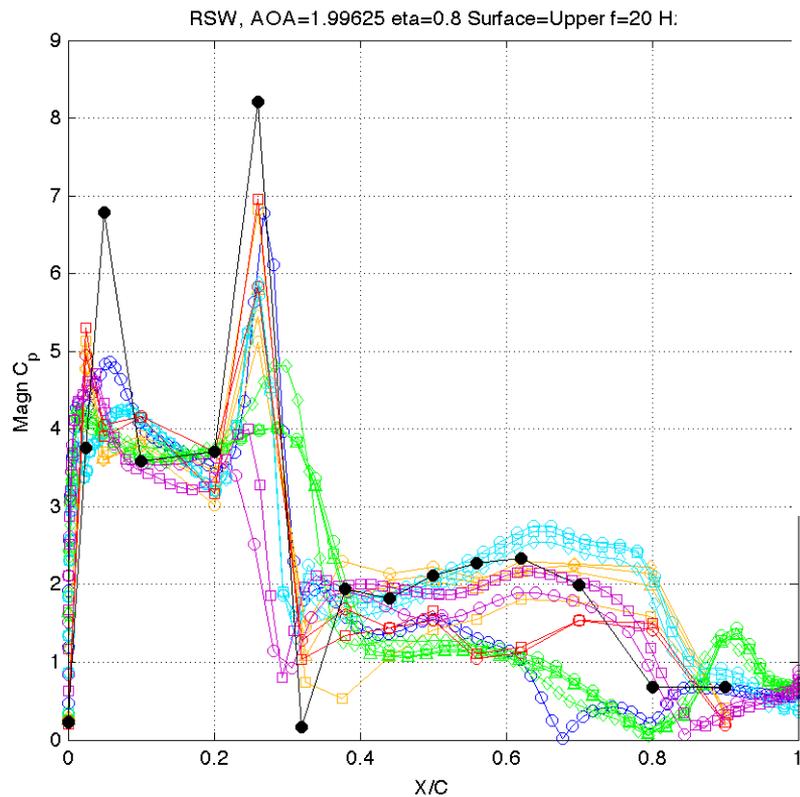
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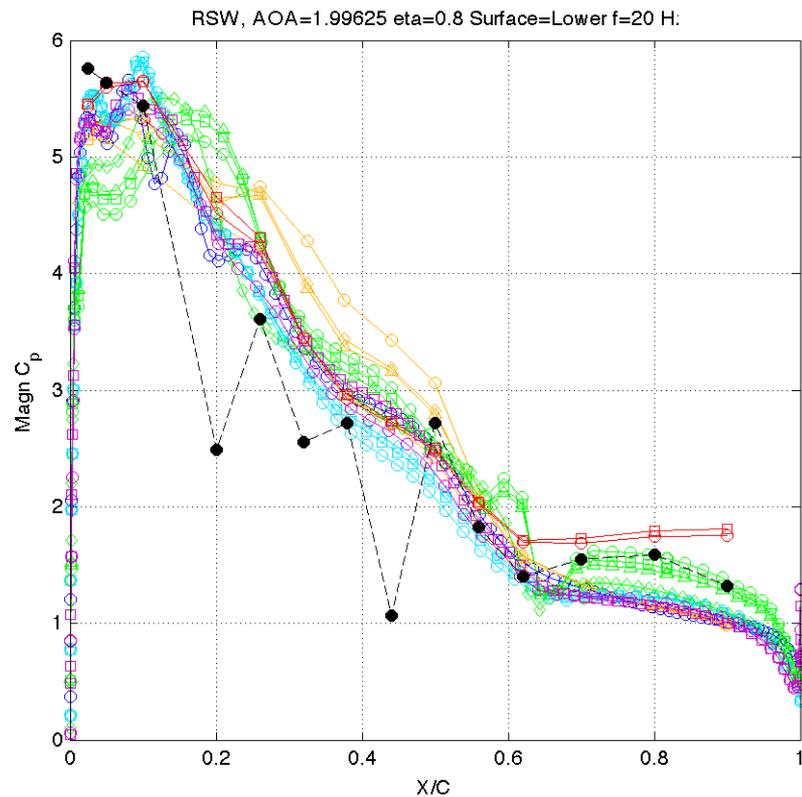
- A Gc
- A Gf
- ◇ A Gm
- B Gc
- B Gf
- ◇ B Gm
- C Gc
- C Gf
- ◇ C Gm
- D Gc
- D Gf
- ◇ D Gm
- E Gc
- E Gf
- ◇ E Gm
- F Gc
- F Gf
- ◇ F Gm
- Exp

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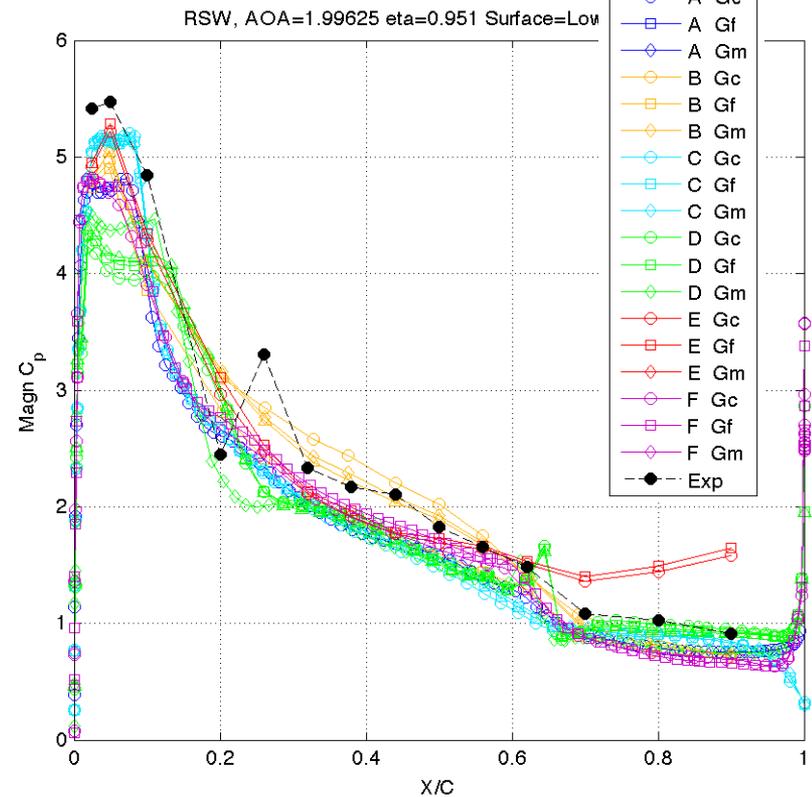
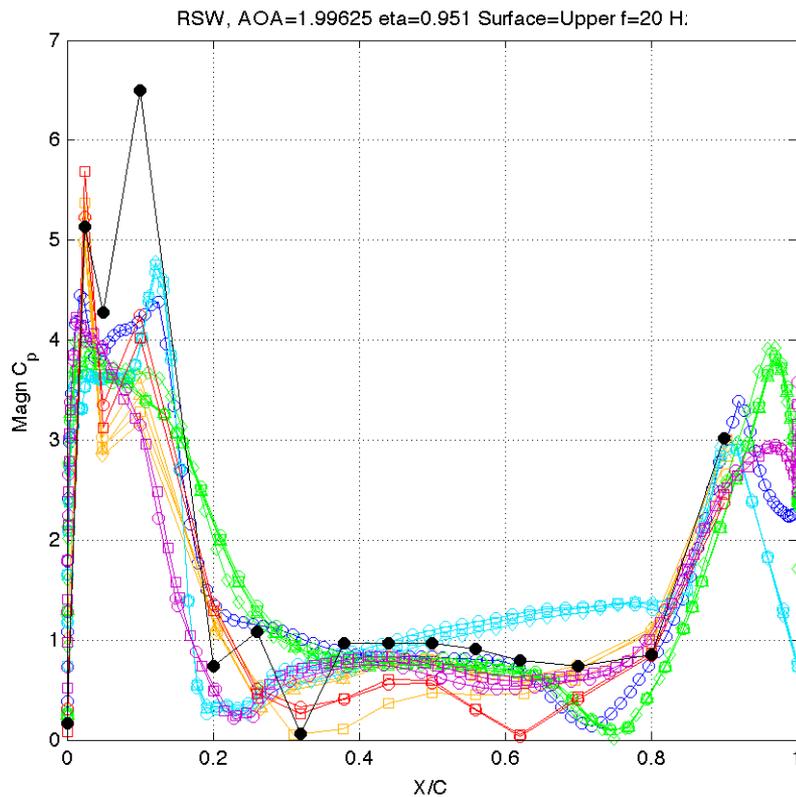


- A Gc
- A Gf
- ◇ A Gm
- B Gc
- B Gf
- ◇ B Gm
- C Gc
- C Gf
- ◇ C Gm
- D Gc
- D Gf
- ◇ D Gm
- E Gc
- E Gf
- ◇ E Gm
- F Gc
- F Gf
- ◇ F Gm
- - - Exp



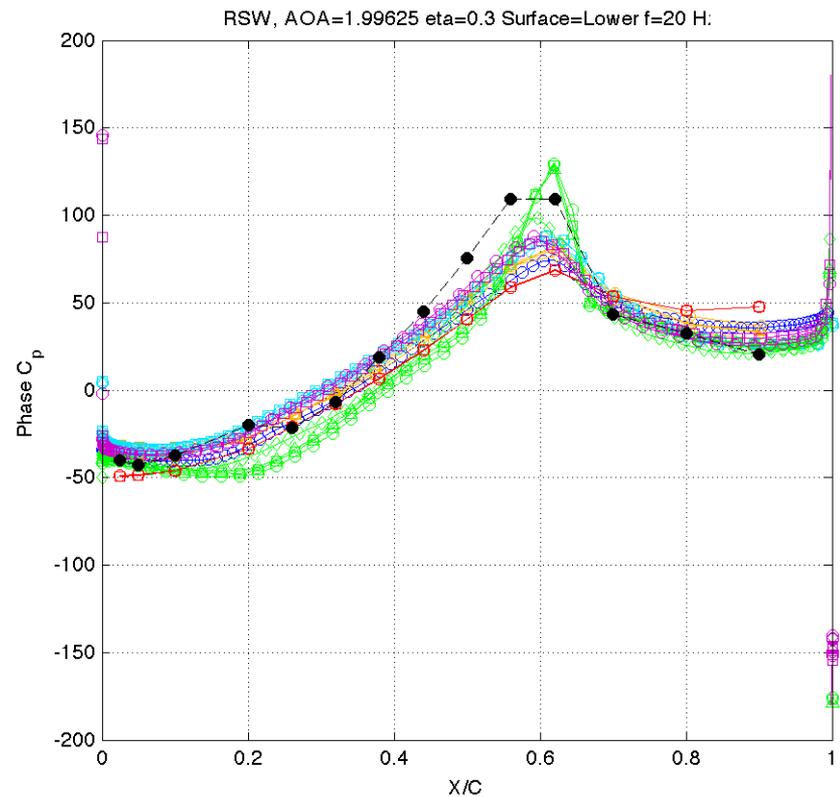
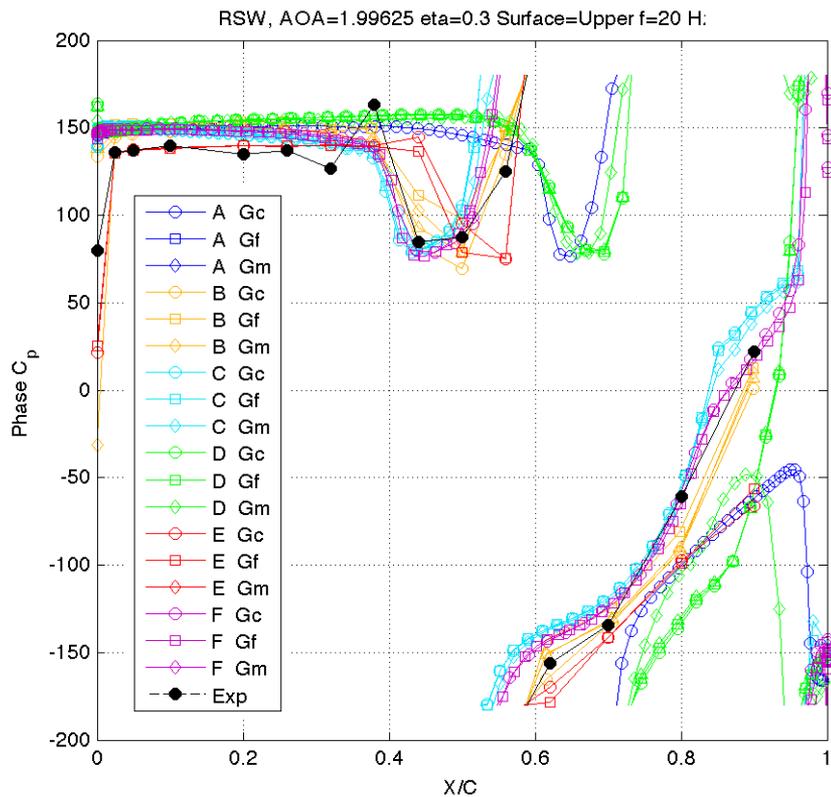
Notes: These comparisons are utilizing the preliminary data, as submitted prior to the AePW. These are workshop results, not publication results. There are significant differences in the geometry used, as well as normalization constants, definitions of FRF and sign conventions. These issues are being sorted out post-workshop. None of the results included should be interpreted without proper consideration of these issues. Corrections and rescalings etc will be performed prior to publication.

# Upper $\eta = 0.951$ Lower



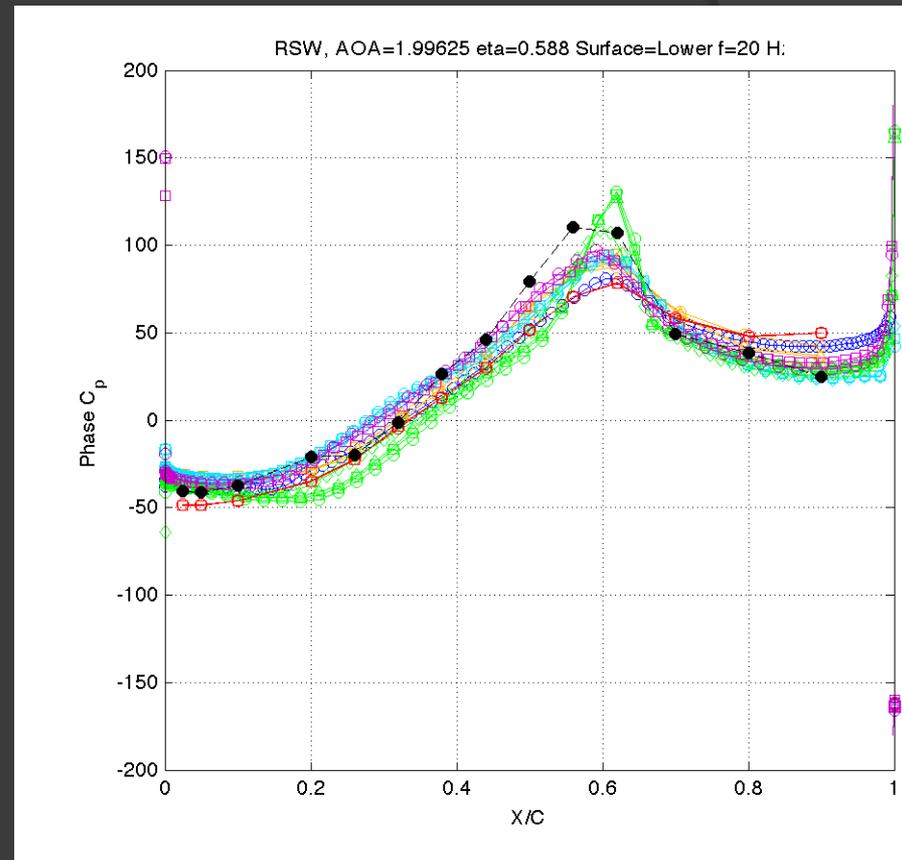
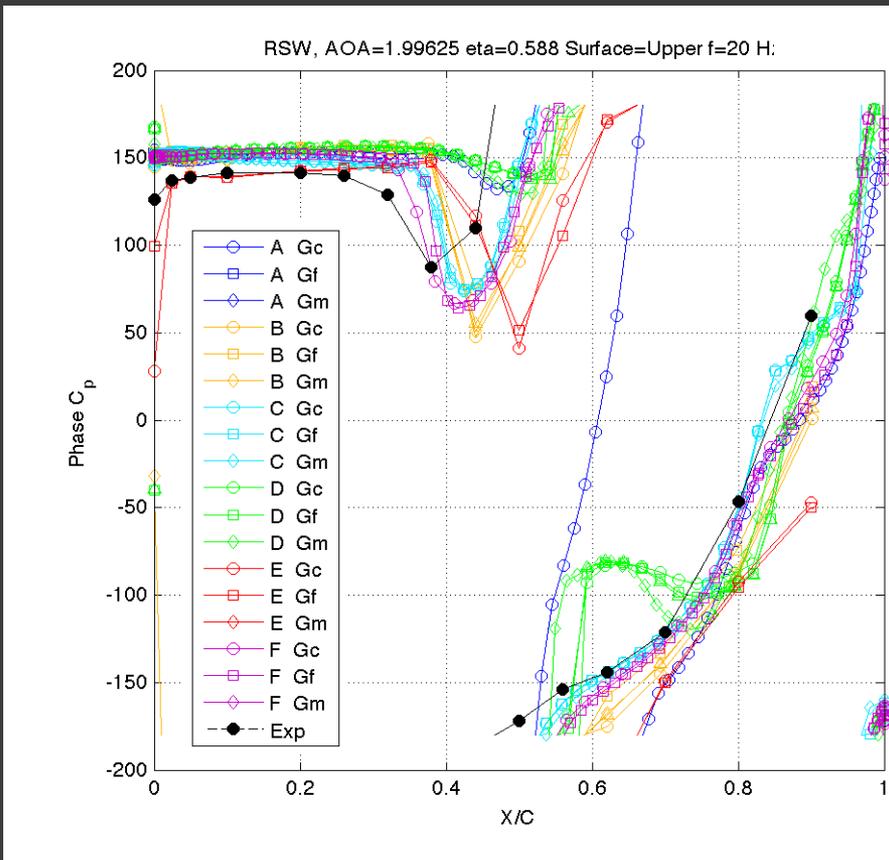
Notes: These comparisons are utilizing the preliminary data, as submitted prior to the AePW. These are workshop results, not publication results. There are significant differences in the geometry used, as well as normalization constants, definitions of FRF and sign conventions. These issues are being sorted out post-workshop. None of the results included should be interpreted without proper consideration of these issues. Corrections and rescalings etc will be performed prior to publication.

# Upper $\eta = 0.309$ Lower



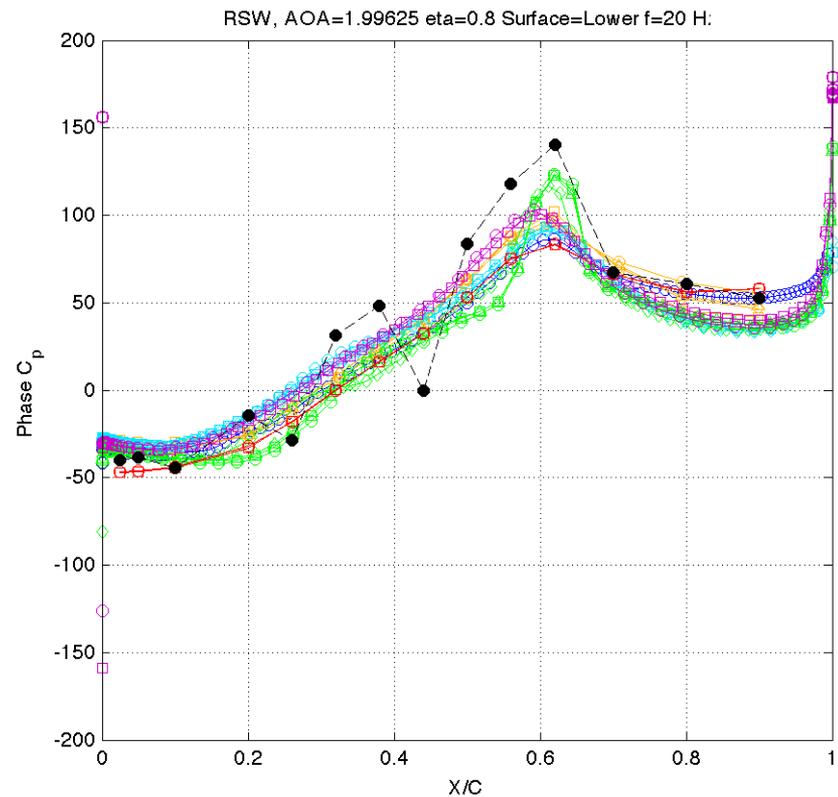
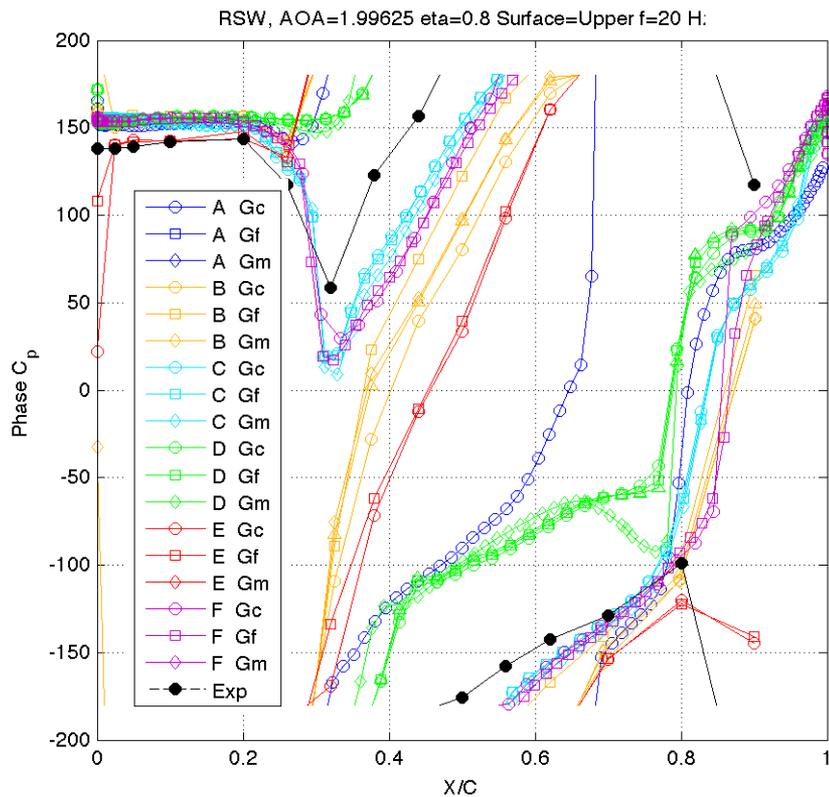
Notes: These comparisons are utilizing the preliminary data, as submitted prior to the AePW. These are workshop results, not publication results. There are significant differences in the geometry used, as well as normalization constants, definitions of FRF and sign conventions. These issues are being sorted out post-workshop. None of the results included should be interpreted without proper consideration of these issues. Corrections and rescalings etc will be performed prior to publication.

# Upper $\eta = 0.588$ Lower



Notes: These comparisons are utilizing the preliminary data, as submitted prior to the AePW. These are workshop results, not publication results. There are significant differences in the geometry used, as well as normalization constants, definitions of FRF and sign conventions. These issues are being sorted out post-workshop. None of the results included should be interpreted without proper consideration of these issues. Corrections and rescalings etc will be performed prior to publication.

# Upper $\eta = 0.809$ Lower



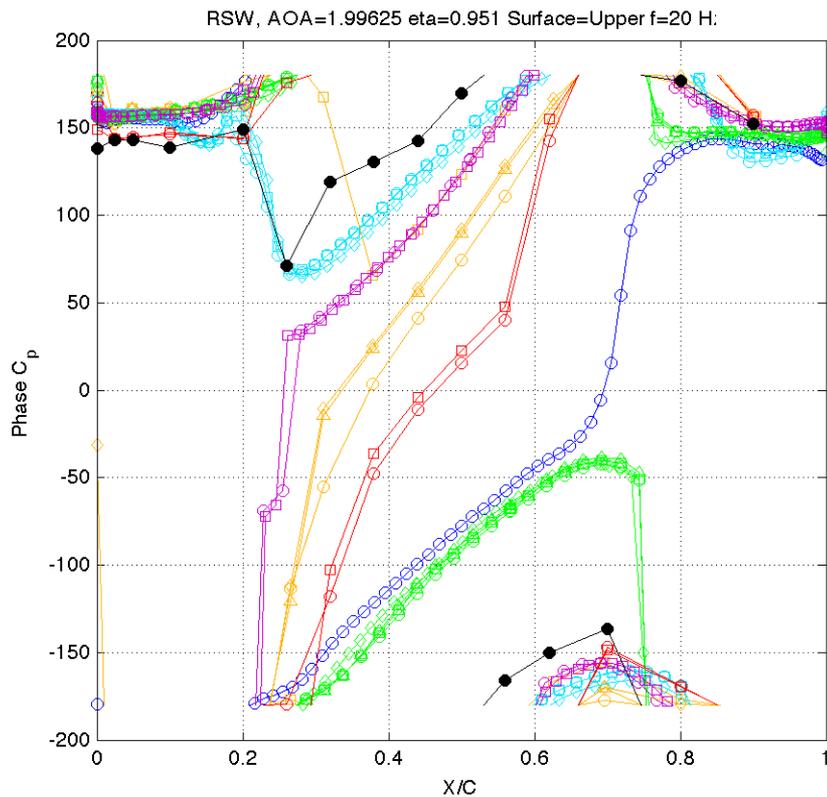
Notes: These comparisons are utilizing the preliminary data, as submitted prior to the AePW. These are workshop results, not publication results.

There are significant differences in the geometry used, as well as normalization constants, definitions of FRF and sign conventions

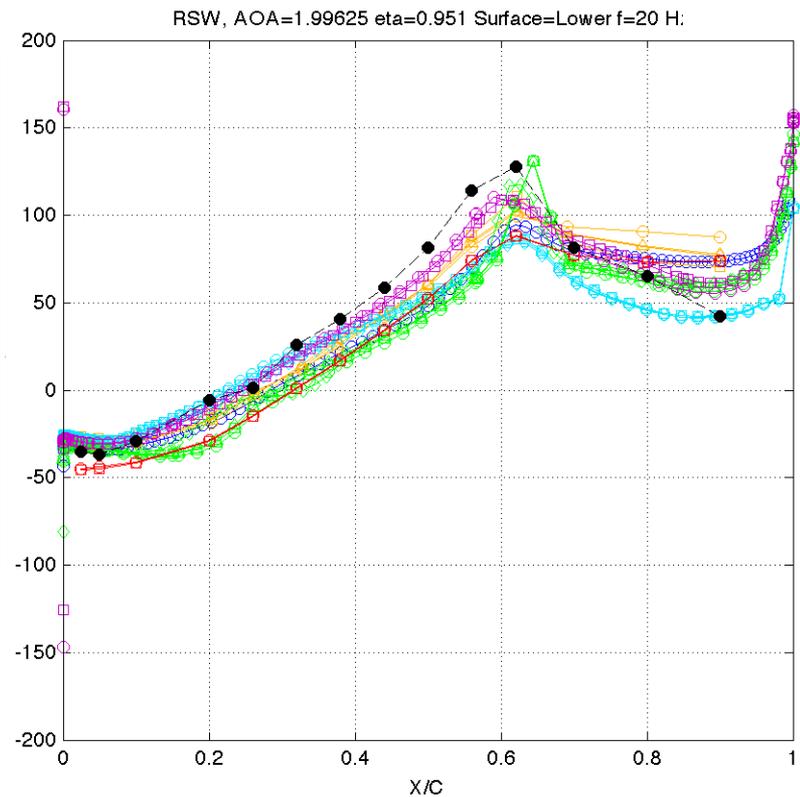
These issues are being sorted out post-workshop. None of the

results included should be interpreted without proper consideration of these issues. Corrections and rescalings etc will be performed prior to publication.

# Upper $\eta = 0.951$ Lower



- A Gc
- A Gf
- ◇ A Gm
- B Gc
- B Gf
- ◇ B Gm
- C Gc
- C Gf
- ◇ C Gm
- D Gc
- D Gf
- ◇ D Gm
- E Gc
- E Gf
- ◇ E Gm
- F Gc
- F Gf
- ◇ F Gm
- Exp



Notes: These comparisons are utilizing the preliminary data, as submitted prior to the AePW. These are workshop results, not publication results. There are significant differences in the geometry used, as well as normalization constants, definitions of FRF and sign conventions. These issues are being sorted out post-workshop. None of the results included should be interpreted without proper consideration of these issues. Corrections and rescalings etc will be performed prior to publication.